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# High-Performance Analog Optical Links

**Photonic Systems, Inc.**

**MIT**

**Sarnoff Corporation**

**Columbia University**

**August 1, 2001**

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**Photonic Systems, Inc.**



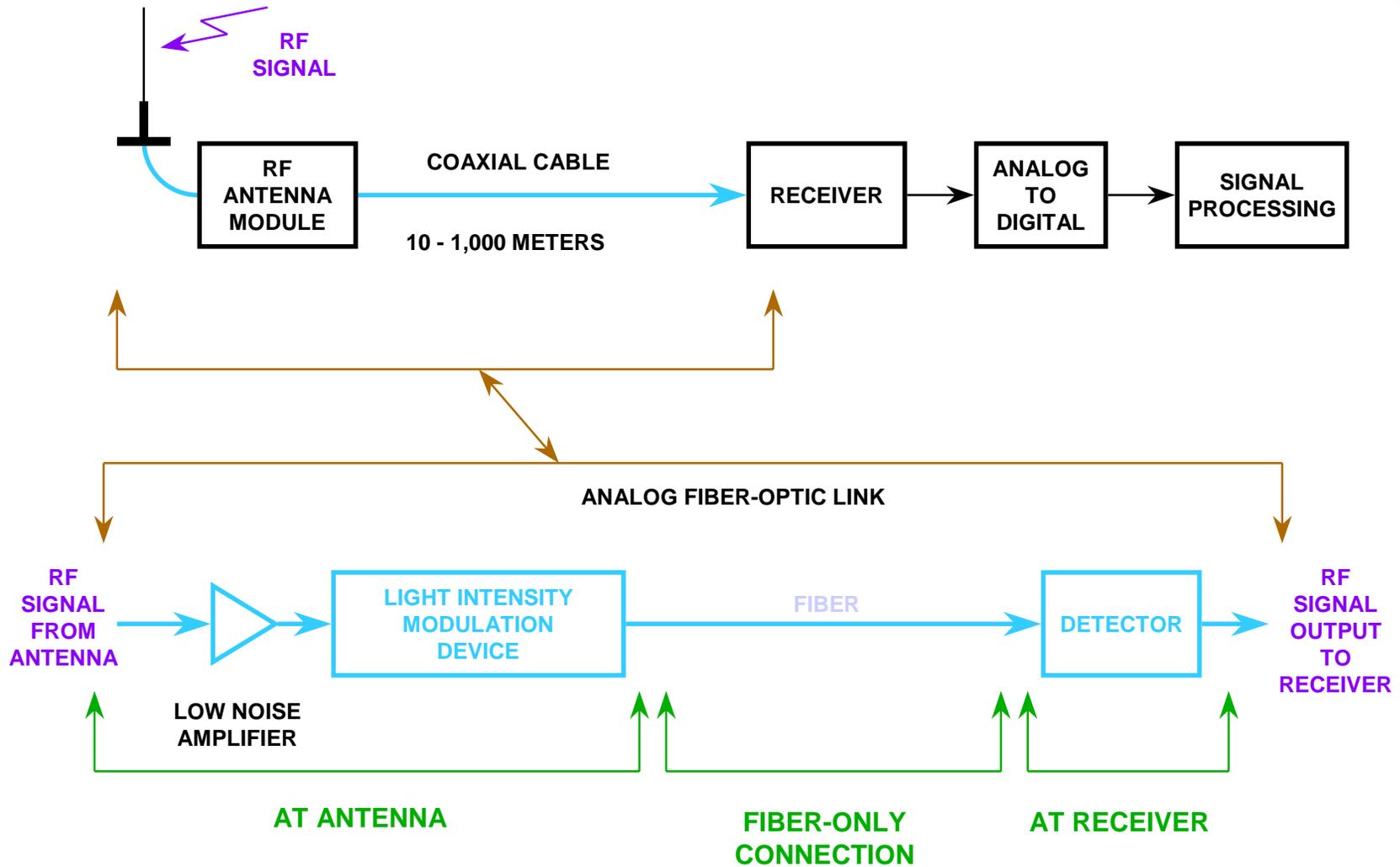
# Outline



- ➔ • **Background**
- **Cascade Laser Development**
- **Resonant Modulator Performance Tradeoffs**
- **Noise/Intermodulation Test Rack**
- **Summary**



# Antenna Remoting Concept



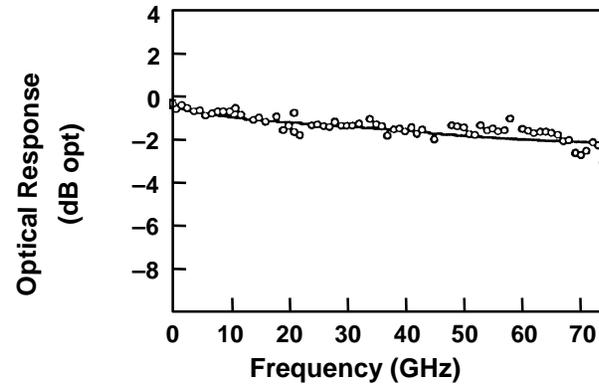
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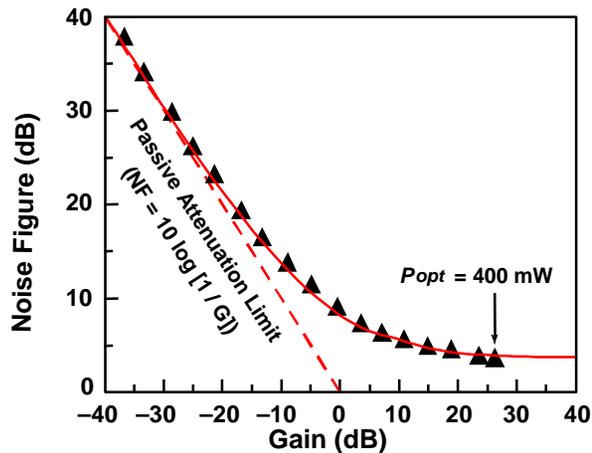
# Record Performance of Analog Links External Modulation



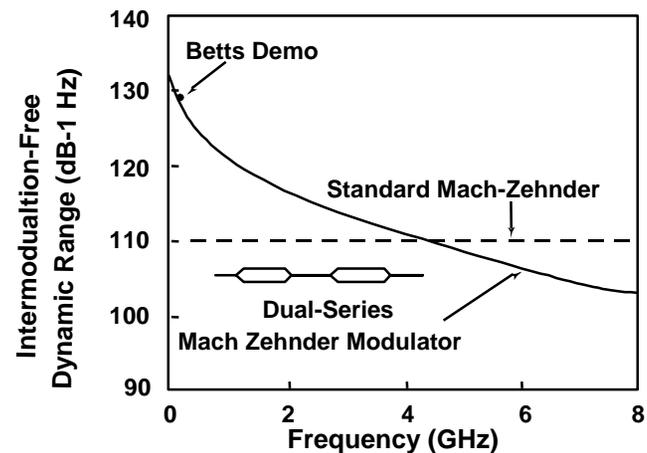
**Record Bandwidth: 75 GHz**  
Noguchi et. al, NTT Opto-Electronic Laboratories  
Noise Figure: 25 dB    Dynamic Range: 110 dB Hz



**Record Noise Figure: 2.5 dB**  
Ackerman & Cox, MIT Lincoln Laboratory  
Bandwidth: 150±10 MHz    Dynamic Range: 110 dB Hz



**Record Dynamic Range: 130 dB**  
Betts, MIT Lincoln Laboratory  
Bandwidth: 200 MHz    Noise Figure: 6 dB



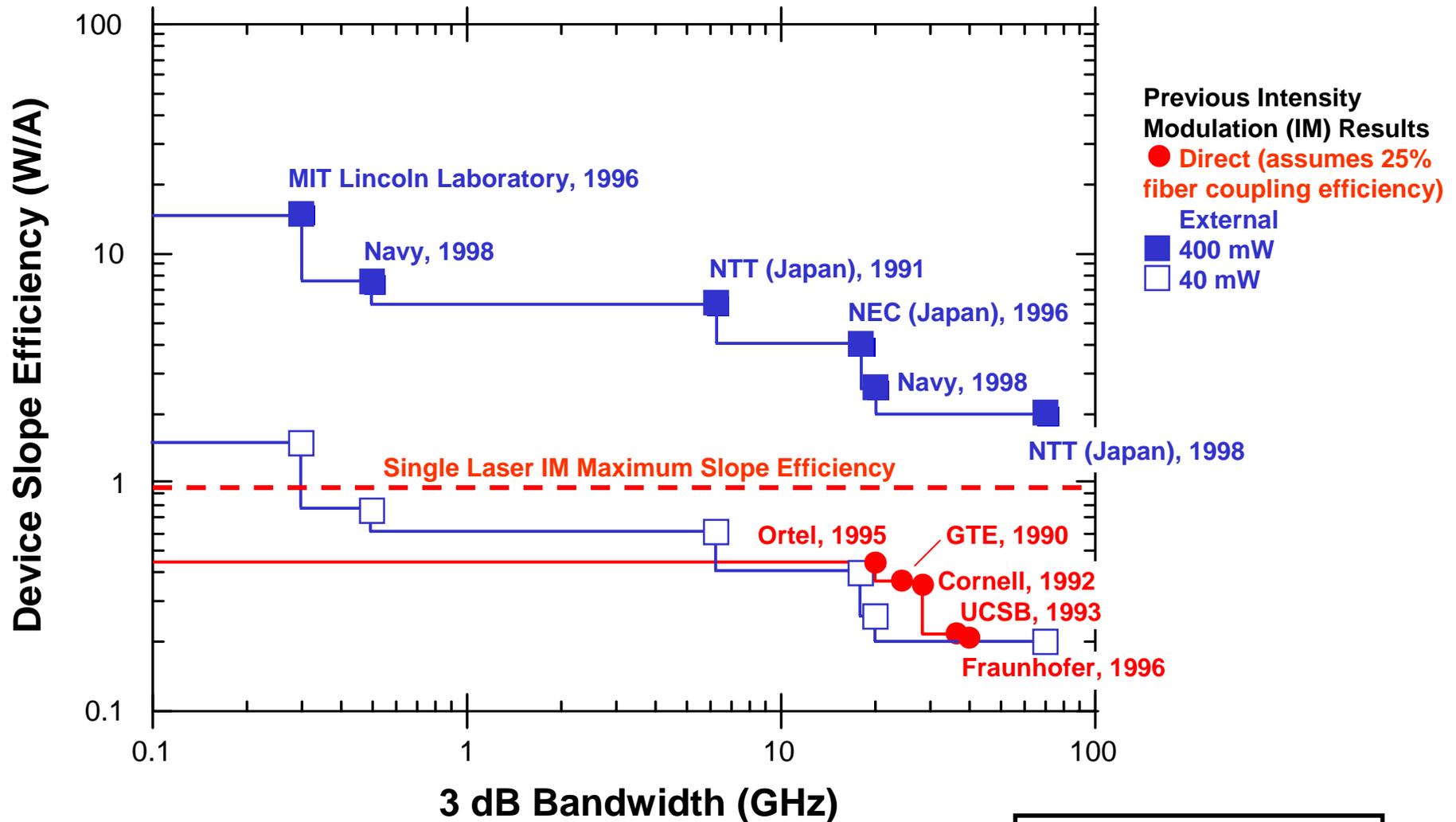
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# Slope Efficiency vs Frequency



Estimates at 1.3  $\mu\text{m}$  Based on Reported Device Parameters



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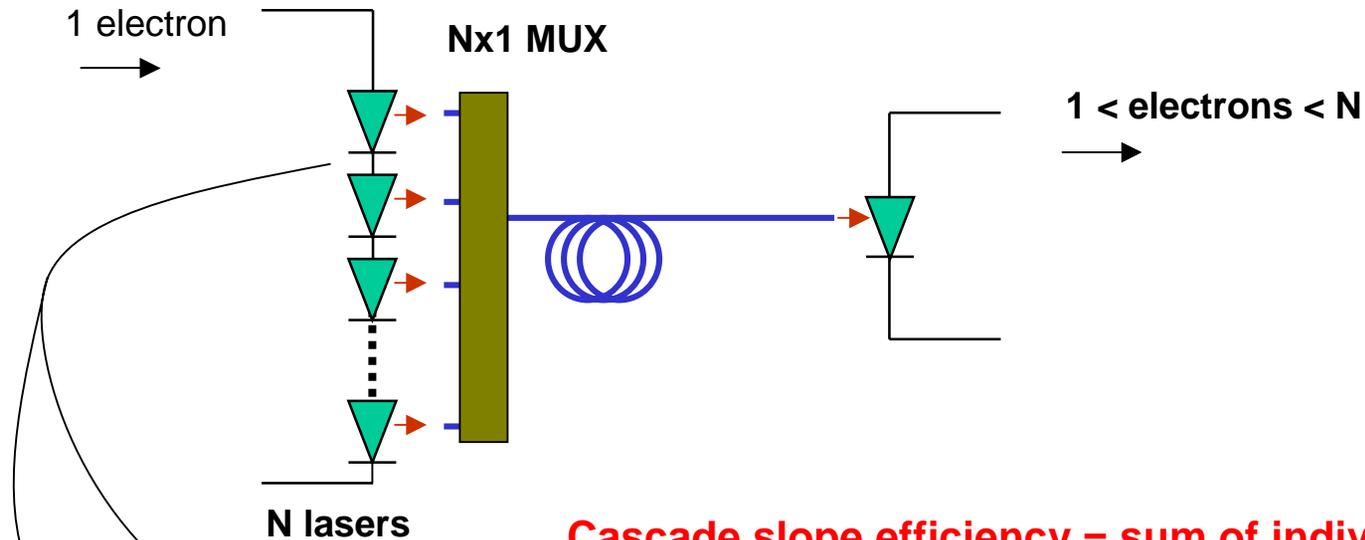
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# Cascade Laser Options



**Cascade slope efficiency = sum of individual laser slope efficiencies**

## Ohmic Connection

- Discrete Cascade
  - Cox et al. 1st demo
- Interconnect Coupled Cascade
  - PSI SBIR Phase II

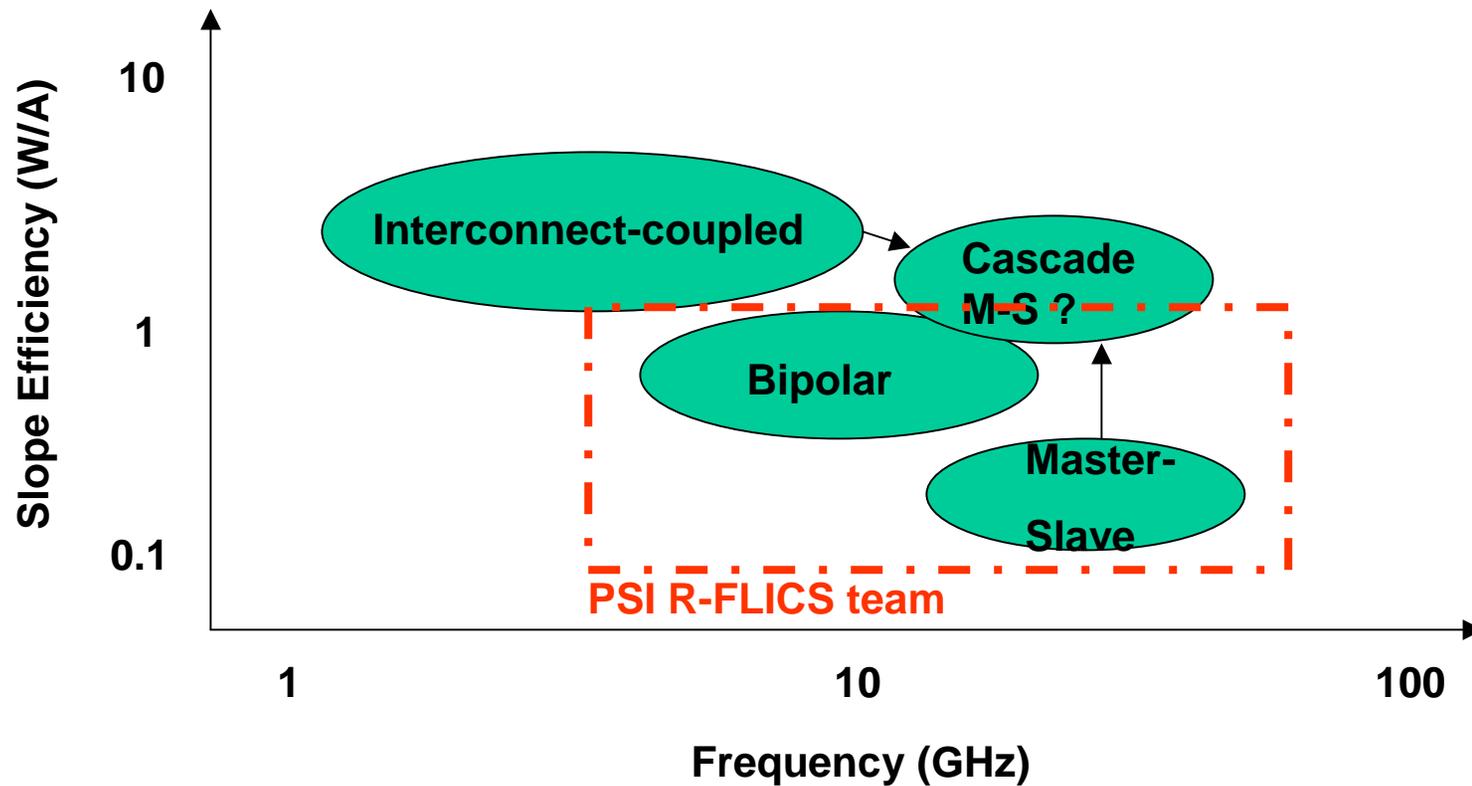
## Tunnel-junction Connection

- Bipolar Cascade
  - PSI R-FLICS team

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# Comparative Performance of Cascade Lasers



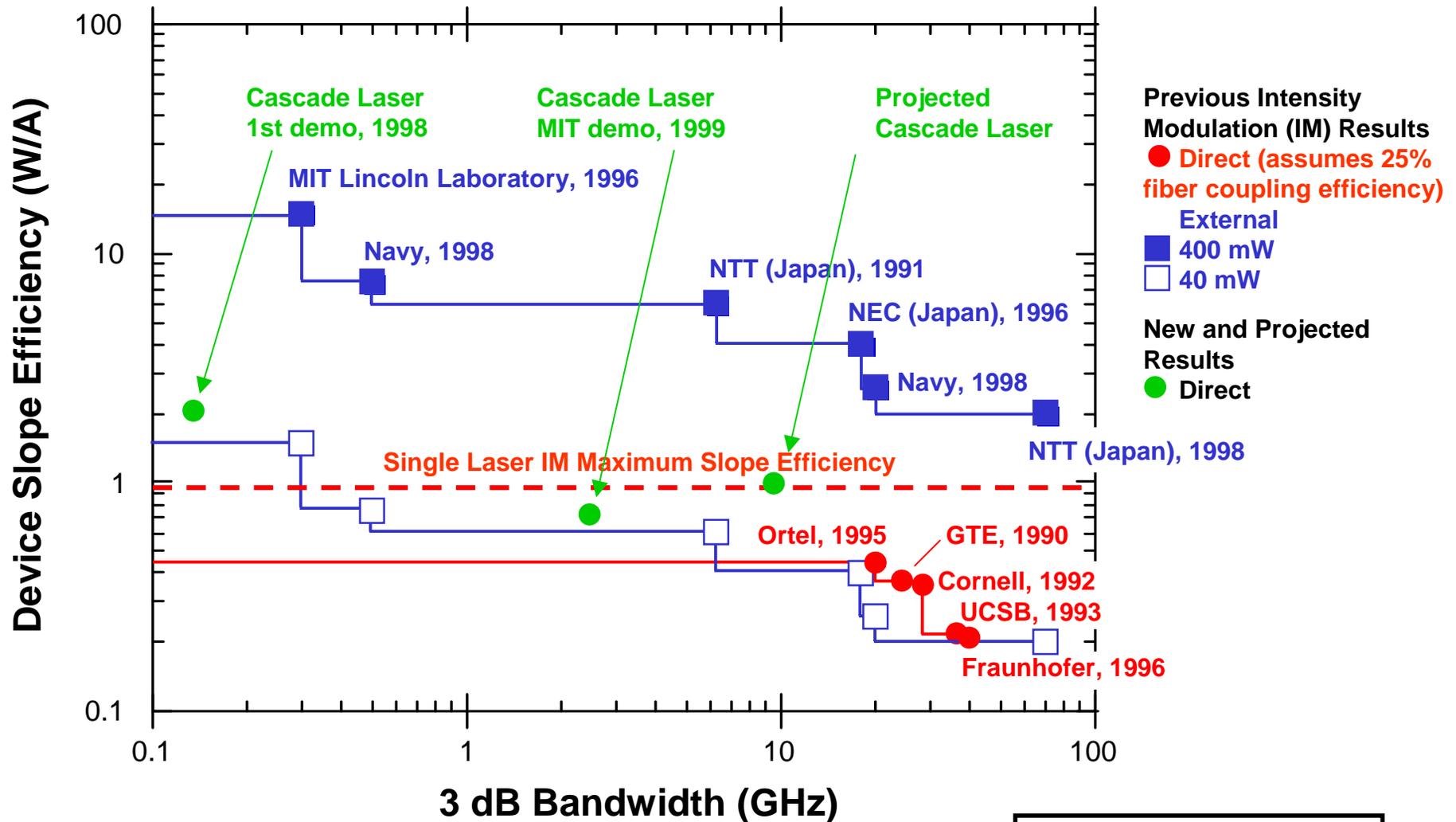
Photonic Systems, Inc.



# Slope Efficiency vs Frequency



Estimates at 1.3  $\mu\text{m}$  Based on Reported Device Parameters



Photonic Systems, Inc.



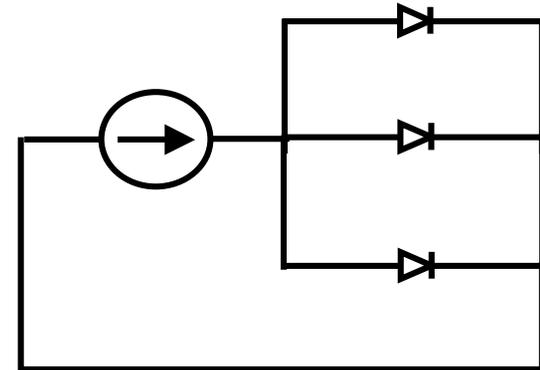
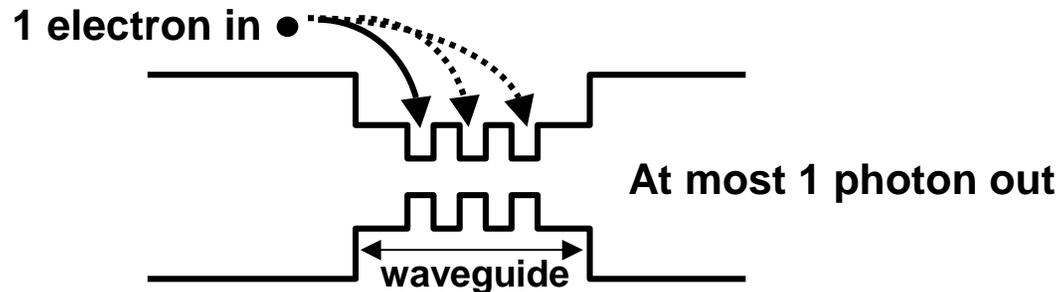
# Outline



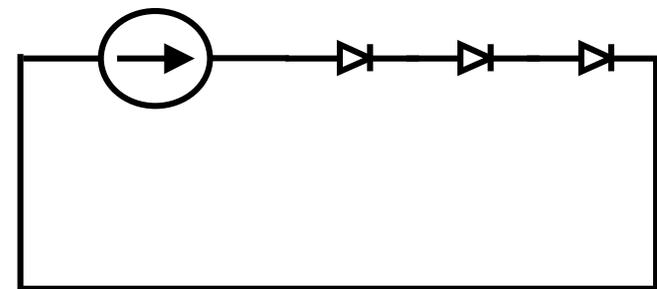
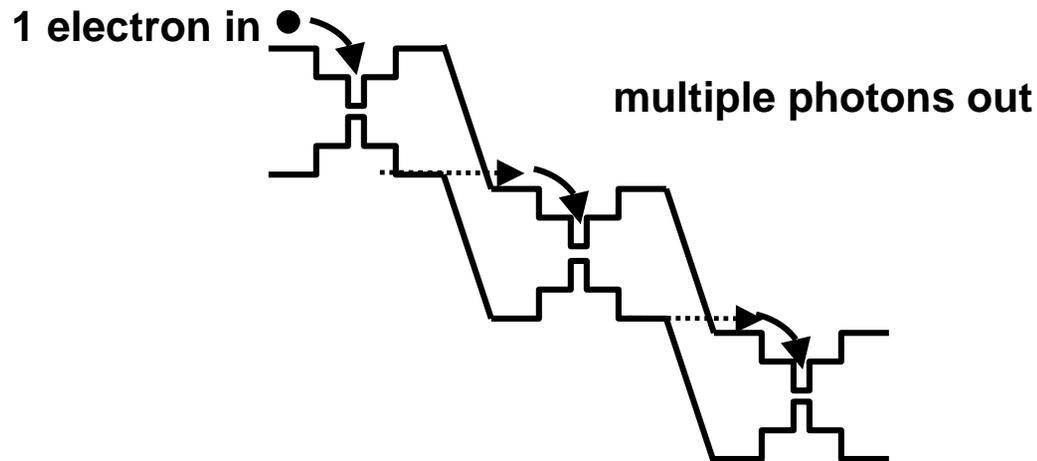
- **Background**
- **Cascade Laser Development**
- ➔ – **Laser design**
  - **1<sup>st</sup> generation**
  - **2<sup>nd</sup> generation**
    - Tunnel junction
    - Fiber coupling
  - **Material growth and characterization**
  - **Resonant modulation and injection locking**
- **Resonant Modulator Performance Tradeoffs**
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# Parallel vs. Series (Cascade) Quantum Well Coupling

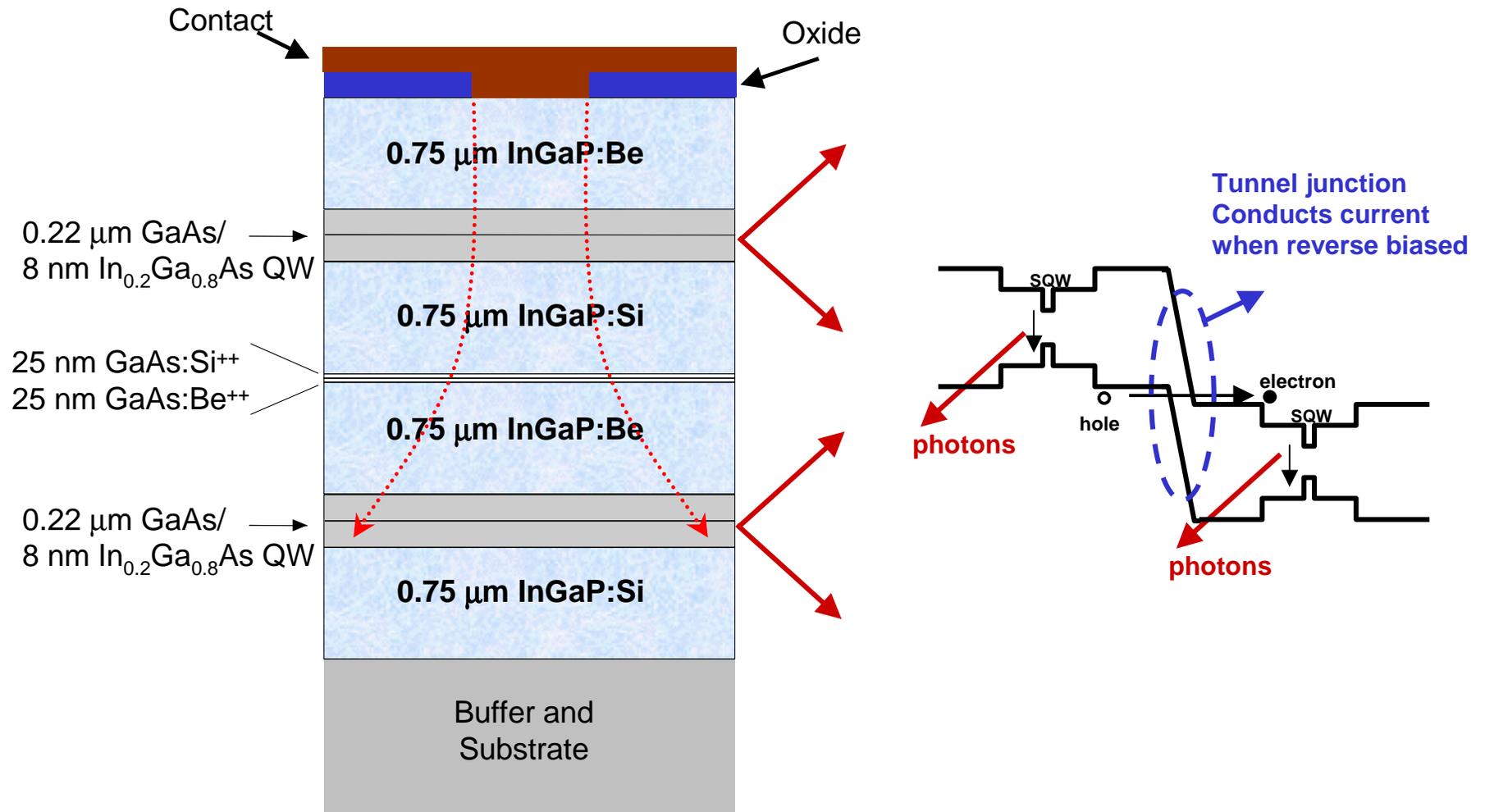
## Parallel Connection



## Series (cascade) Connection



# Bipolar Cascade Laser

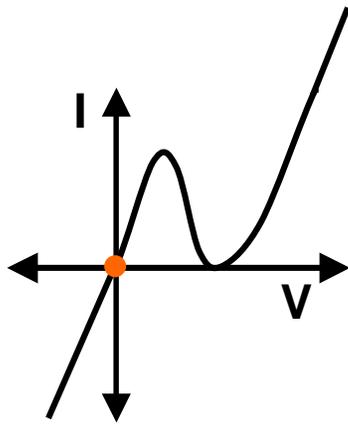
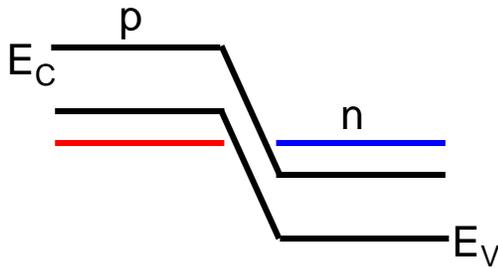


# Second Generation Bipolar Cascade

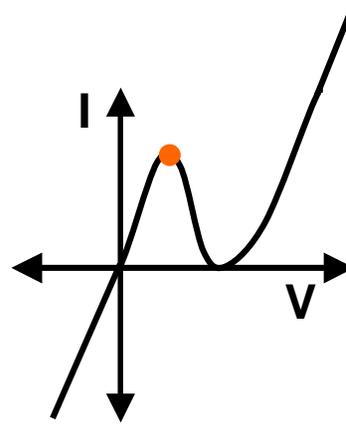
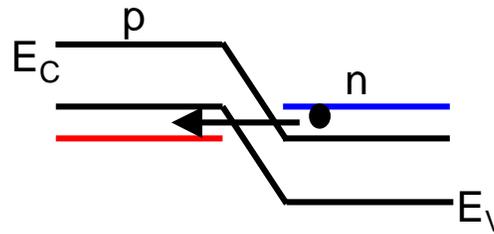
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	<b>1<sup>st</sup> Generation</b>	<b>2<sup>nd</sup> Generation (RFLICS)</b>
• <b>Wavelength</b>	<b>980</b>	<b>1550</b>
• <b>Material System</b>	<b>GaAs</b>	<b>InP</b>
• <b>Waveguides</b>	<b>Uncoupled</b>	<b>ARROW</b>
• <b>Fiber coupling</b>	<b>No</b>	<b>Yes</b>
• <b>Number of laser junctions</b>	<b>2</b>	<b>3</b>

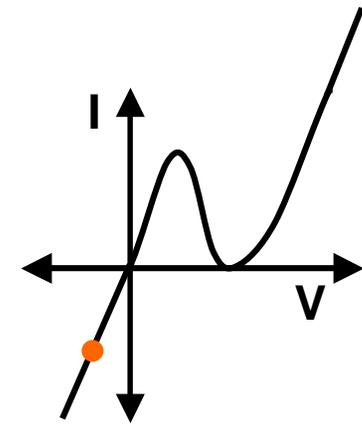
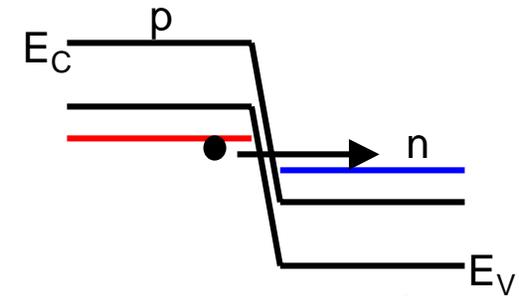
# The Tunnel Junction



*Equilibrium Junction:*  
n- and p-sides  
degenerately doped



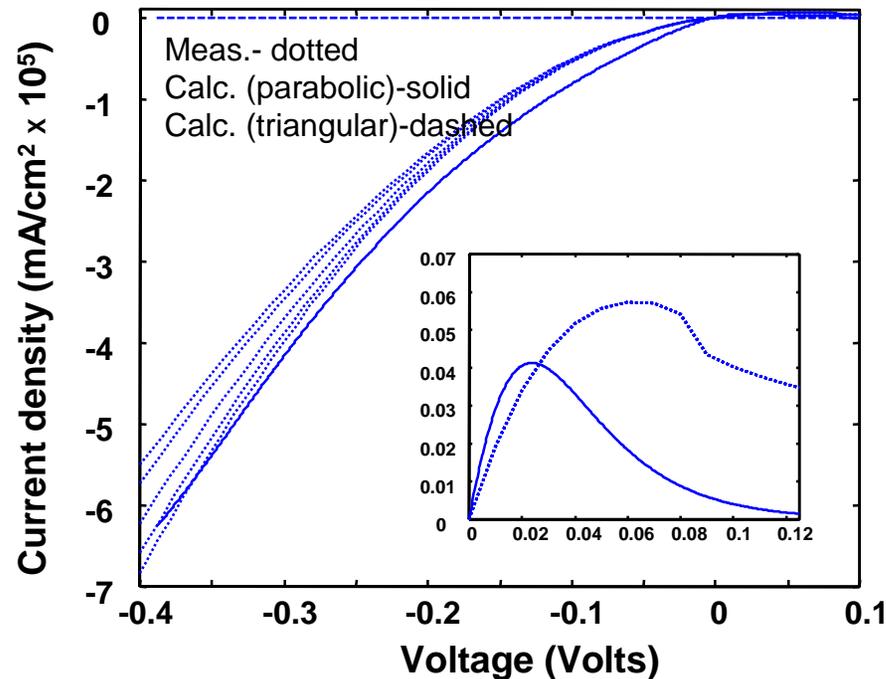
*Peak Forward Bias Current:*  
Maximum alignment of  
unoccupied states on p-side  
with occupied states on n-side.



*Reverse Biased Junction:*  
Monotonically increasing current  
with applied bias.

Region of operation for  
cascade laser.

# Measurement and Calculation of Tunneling Current



There is good agreement between the calculated and measured characteristics.

- Doping of test structure:

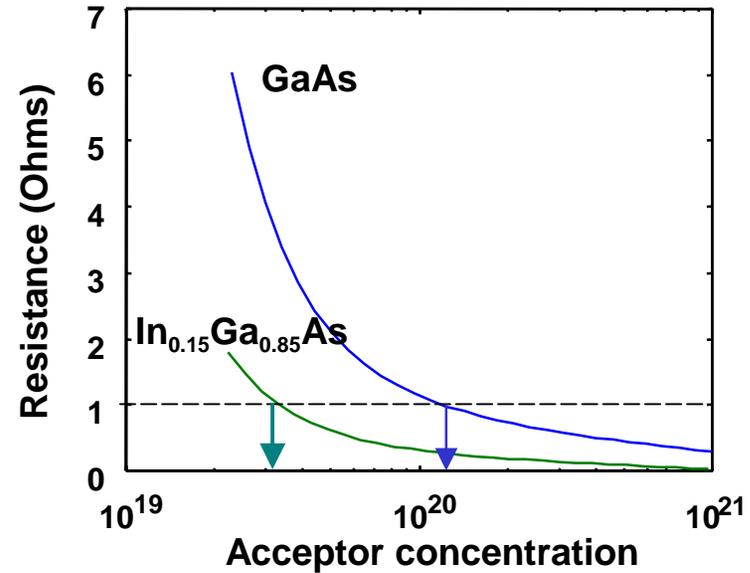
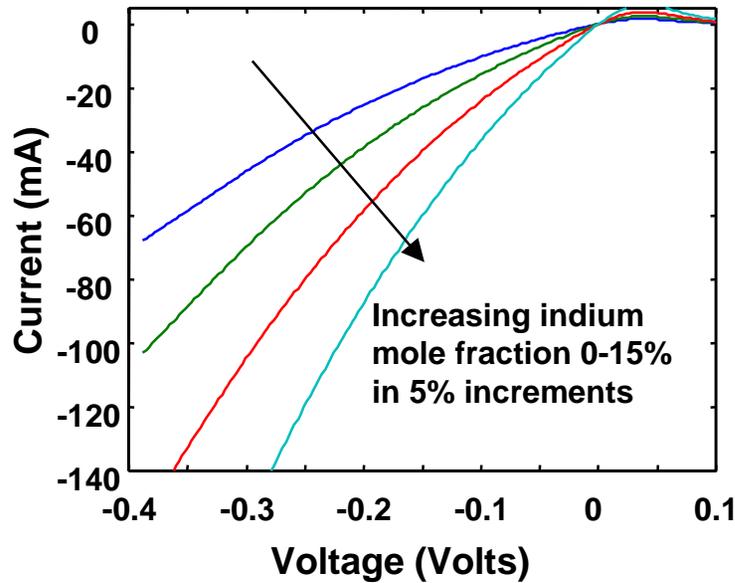
$$N_A = 8 \times 10^{18} \text{ cm}^{-3}, N_D = 1 \times 10^{19} \text{ cm}^{-3}$$

- Test structures were 20 to 100  $\mu\text{m}$  diameter posts

- Measurements done on an HP4145 semiconductor parameter analyzer

- Measured values for the contact and substrate resistance were subtracted from the measured I-V curve ( $5 \cdot 10^{-4} \Omega \cdot \text{cm}^2$ ,  $4.5 \Omega$ ).

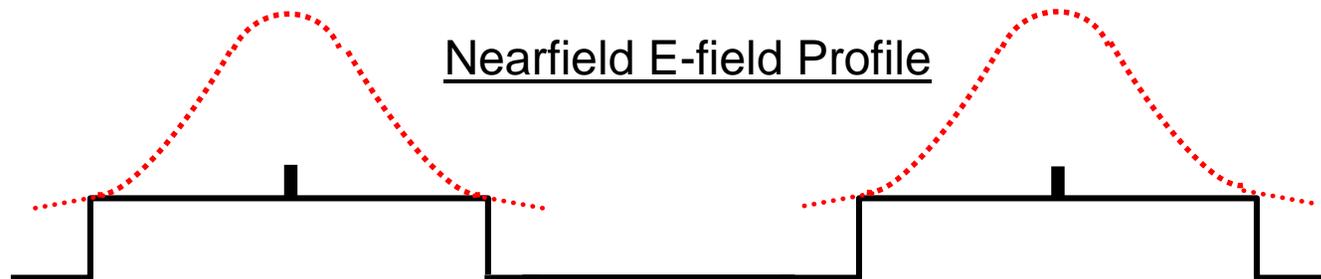
# Effect of In Mole Fraction on Tunneling Characteristics



	<u>GaAs</u>	<u>In<sub>0.15</sub>Ga<sub>0.85</sub>As</u>
Bandgap	1.42 eV	1.28 eV
Effec. mass	0.067 m <sub>o</sub>	0.052 m <sub>o</sub>

Donor and acceptor doping  $2 \times 10^{19}$   
 Device size  $20 \mu\text{m} \times 500 \mu\text{m}$

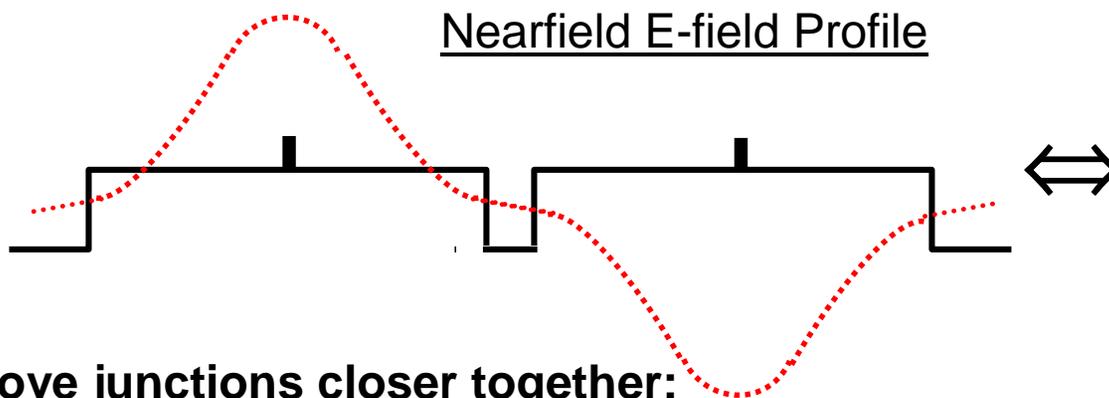
# Coupling Into Fiber



**1<sup>st</sup> Generation Bipolar cascade:**

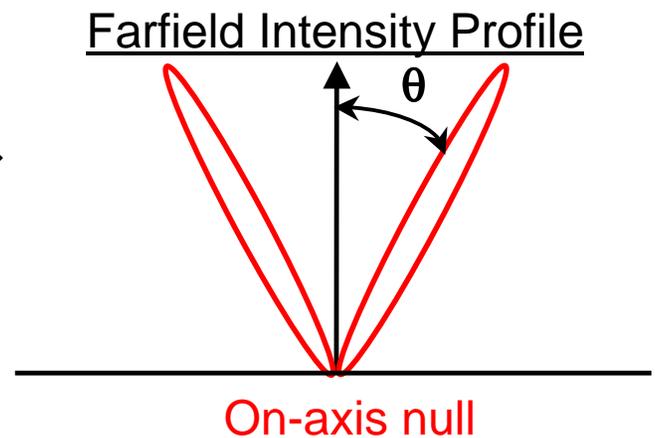
- Multiple waveguides are optically uncoupled
- Output fields of two guides are incoherent

**IN EITHER CASE  
CAN'T COUPLE INTO  
SINGLE MODE FIBER**



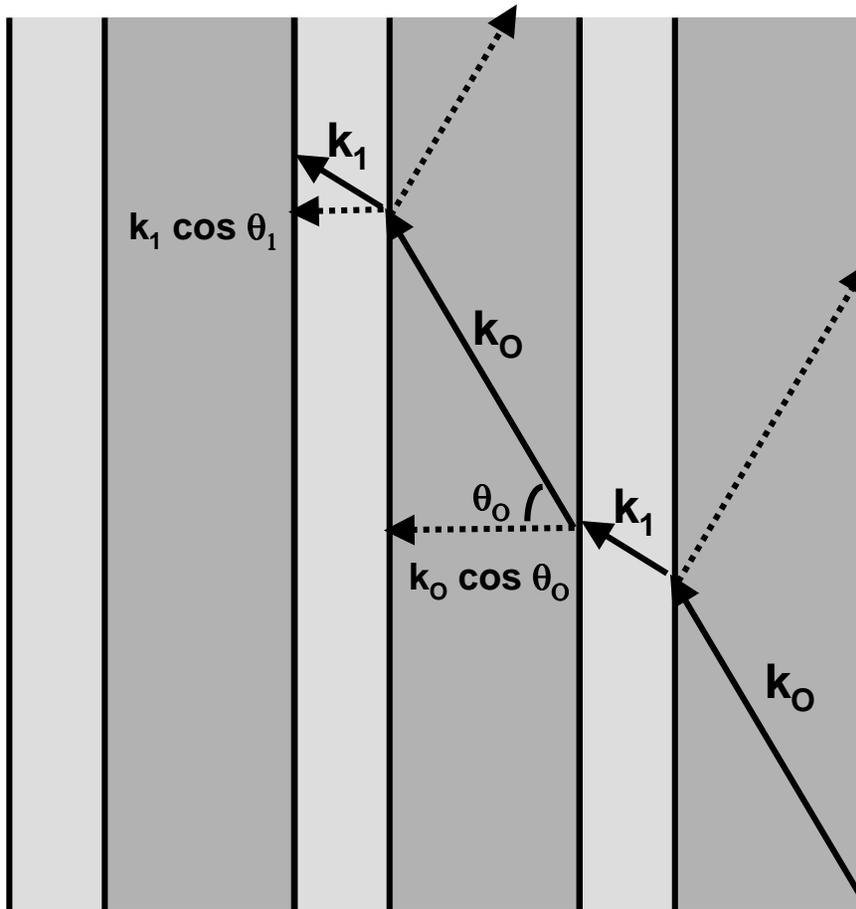
**Move junctions closer together:**

- Increases losses from tunnel junction.
- The fundamental lasing mode is out of phase.



# Guiding and Anti-Guiding Waveguides

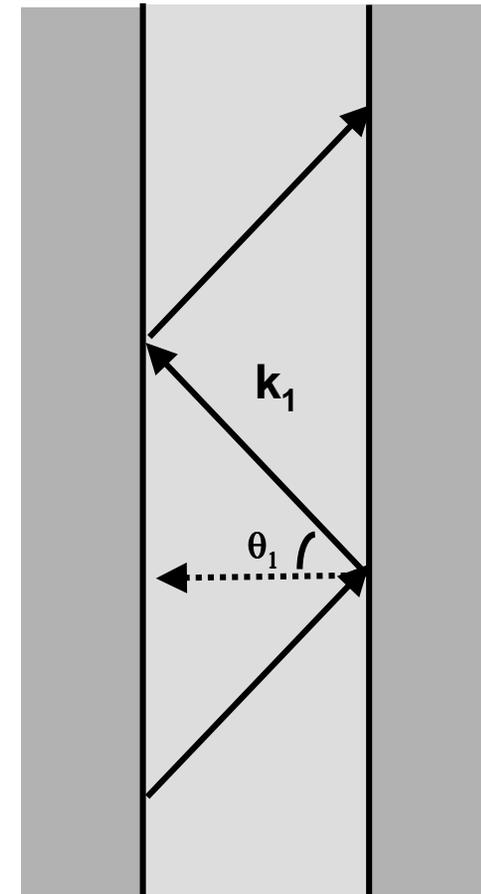
Anti-guiding (ARROW) Waveguide



$$k_0 \cos \theta_0 = \pi \text{ or equivalently } d = \lambda_0 / 2$$

$$k_1 \cos \theta_1 = \pi \text{ or equivalently } s = \lambda_1 / 2$$

Guided Waveguide



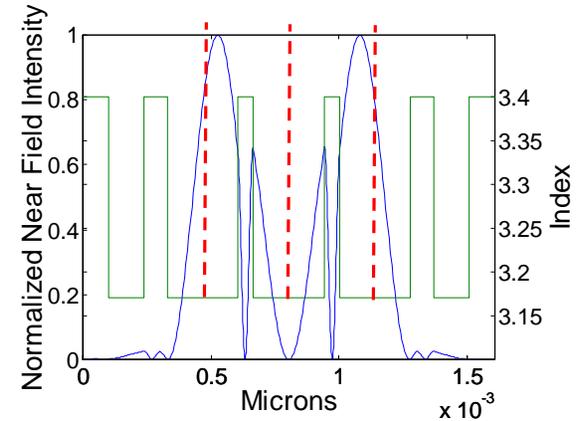
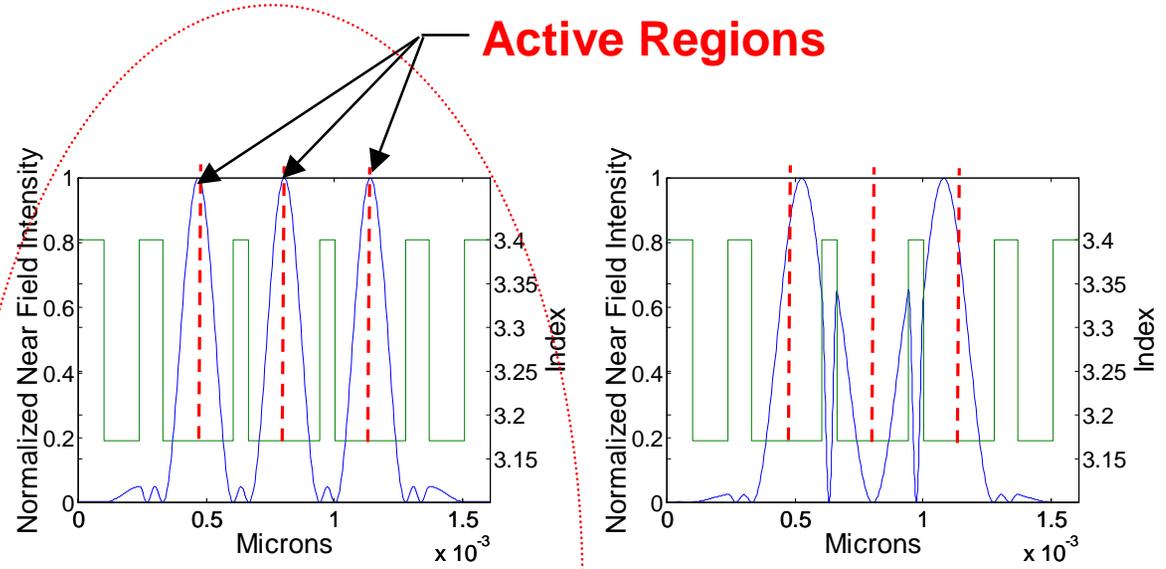
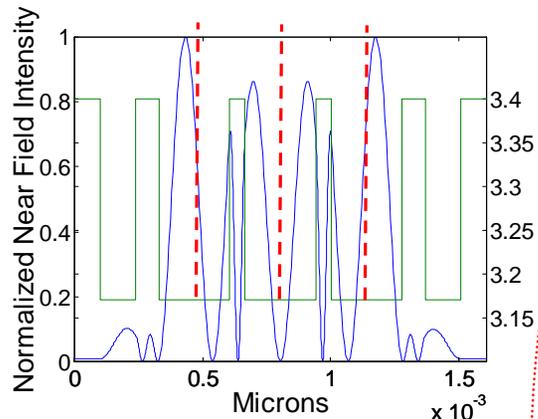
$$\theta_1 > \theta_c$$

Low Index

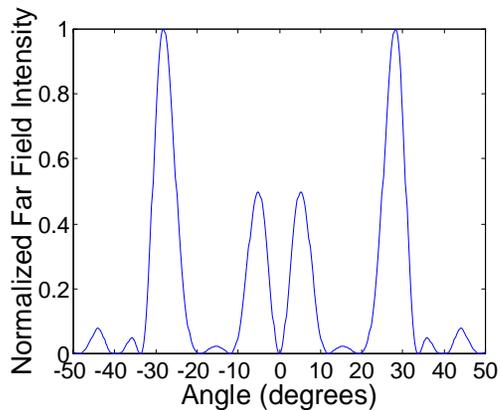
High Index

# Bipolar ARROW Cascade: Near and Far Field

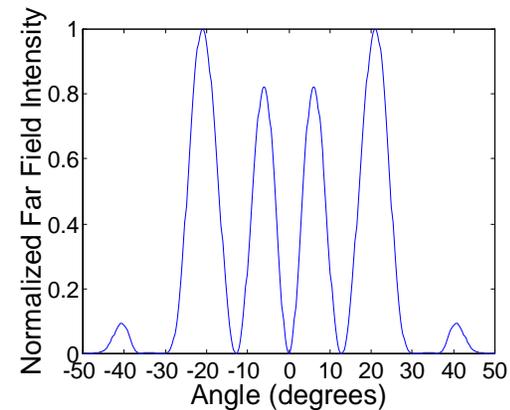
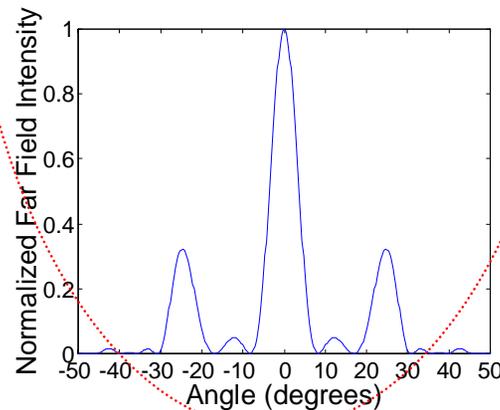
## Near Field:



## Far Field:



60% power in center lobe

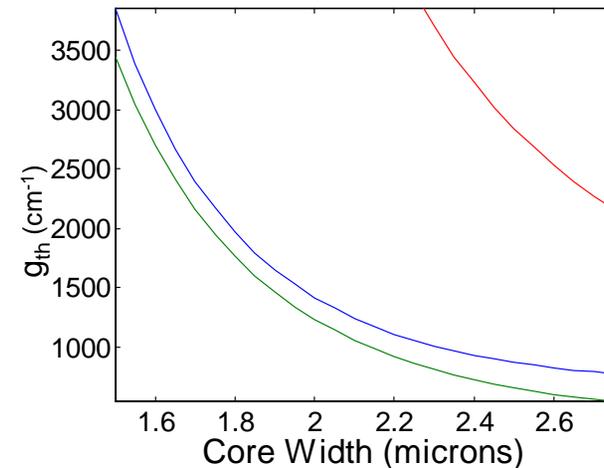


# Bipolar ARROW Cascade: Threshold Gain & Current

## Threshold gain ( $g_{th}$ ):

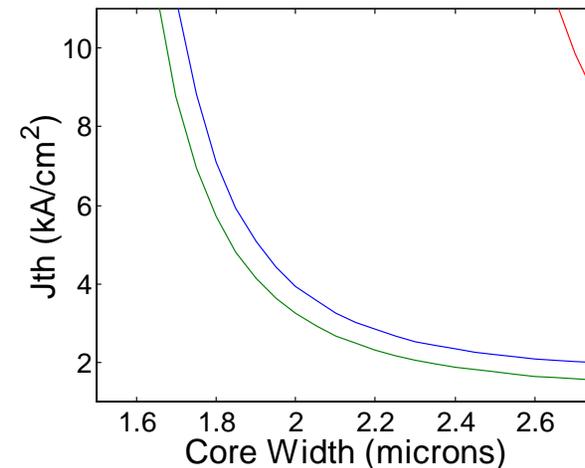
$$\Gamma g_{th} = \langle \alpha_i \rangle + \alpha_m + \alpha_r$$

- $\langle \alpha_i \rangle$  = absorption loss
- $\alpha_m$  = mirror loss
- $\alpha_r$  = radiation loss
- $g_{th}$  decreases with increasing core width



## Threshold current density ( $J_{th}$ ):

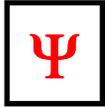
- $J_{th}$  decreases with increasing core width
- Lowest threshold current achieved for fundamental mode



# Material Growth

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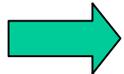
- **Outside growth**
  - **Outside material facilitates technology transfer**
  - **Turn around too slow for design purposes**
    - **Submitted PO for tunnel junction material 1/00, received 8/00**
    - **Submitted PO for ARROW structure 3/00, still have not received 15 months later**
  - **Reviewing alternatives to achieve technology transfer objective**
- **MIT growth**
  - **Switched emphasis to in-house grown material for design phase**
  - **Have completed ~ 30 runs, about 2/week**
  - **Material quality and turn around time will support laser design schedule**



# Outline



- **Background**
- **Cascade Laser Development**
  - **Laser design**
    - **1<sup>st</sup> generation**
    - **2<sup>nd</sup> generation**
      - Tunnel junction
      - Fiber coupling
  - **Material growth and characterization**
  - **Resonant modulation and injection locking**
- **Resonant Modulator Performance Tradeoffs**
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# Background

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## Detuned Loading (1 laser on different sides of DBR)

- K. Vahala, et al., 1985 → 1.6 x bandwidth enhancement to 2.5GHz, reduced phase noise
- O. Kjebon, et al., 1997 → 31GHz direct modulation bandwidth

## Injection Locking (2 FP lasers with master locking slave)

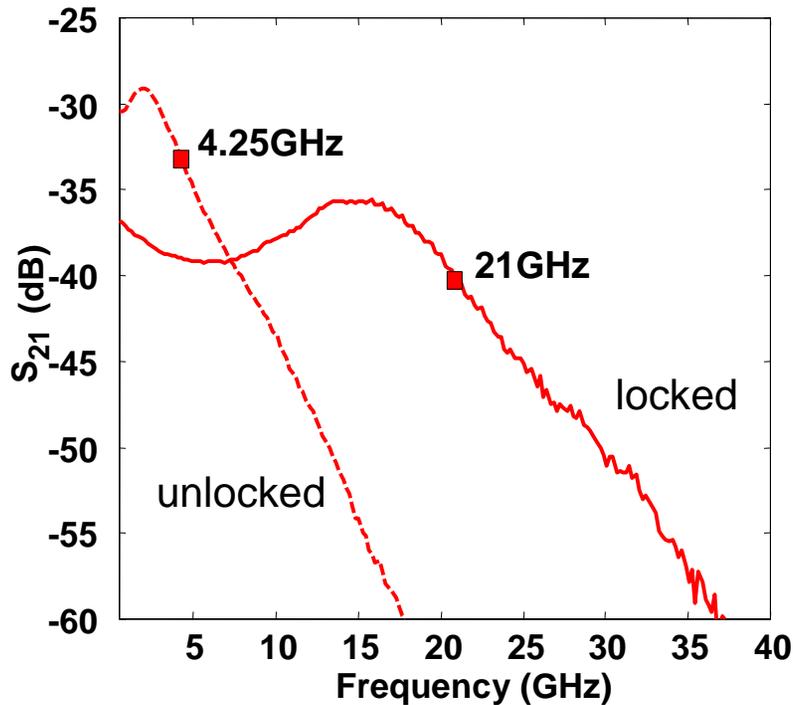
- X. J. Meng, et al., 1998 → 3.7 x bandwidth enhancement to 15GHz
- N. A. Olsson, et al., 1985 → 2Gb/s chirp free transmission over 82.5km SMF

## Resonant Modulation (2 DBR lasers)

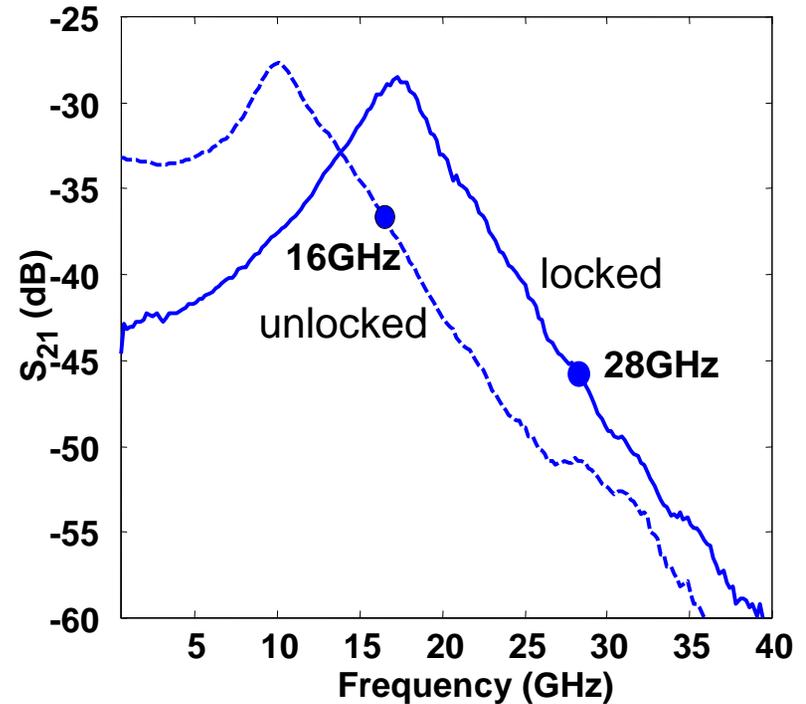
Incorporate both effects by injection locking DBR lasers for high bandwidth and low chirp.

# Resonant Modulation Bandwidth Enhancement

**-1.9dB Injection Ratio (11mA bias)**

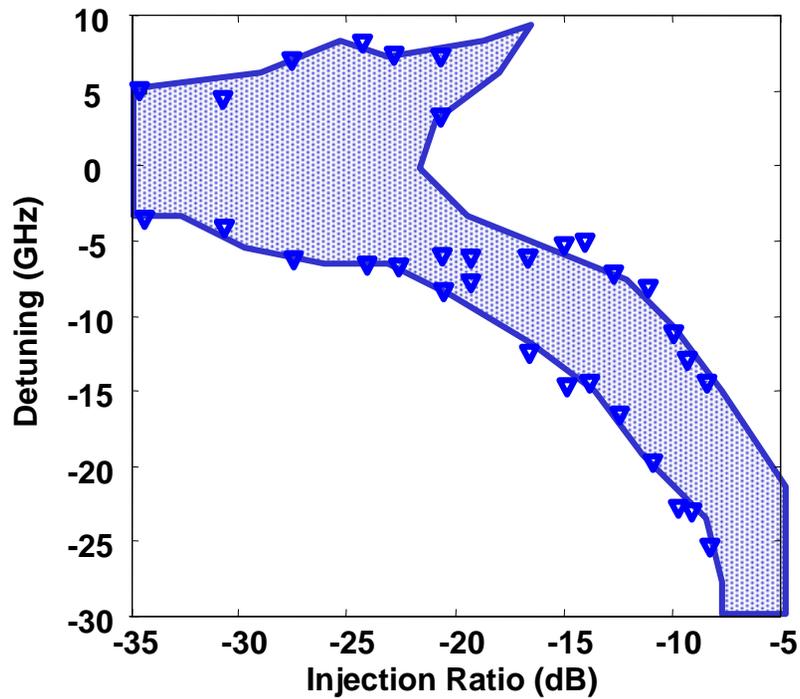


**-11.8dB Injection Ratio (60mA bias)**

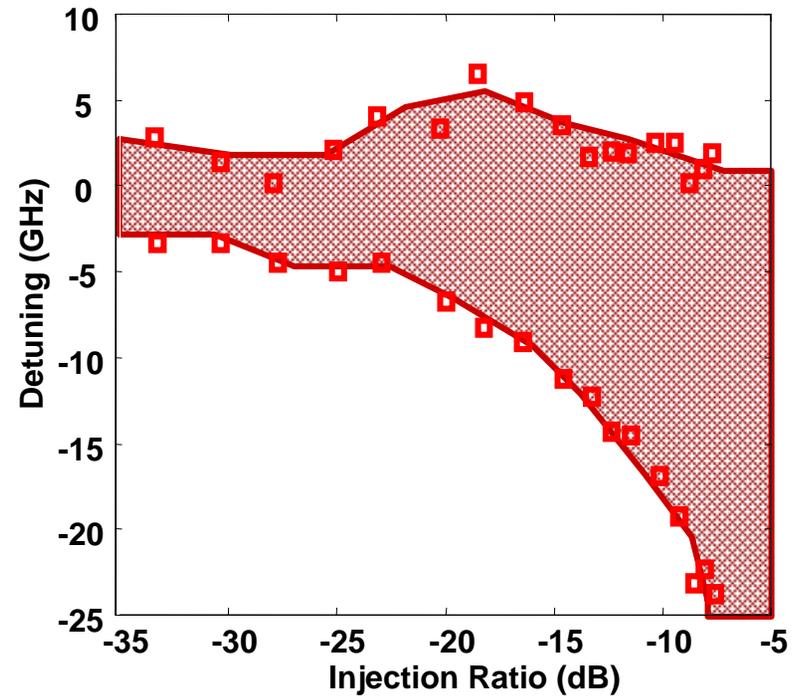


$$\text{Injection Ratio: } \frac{\text{Injected Master power}}{\text{Slave power}}$$

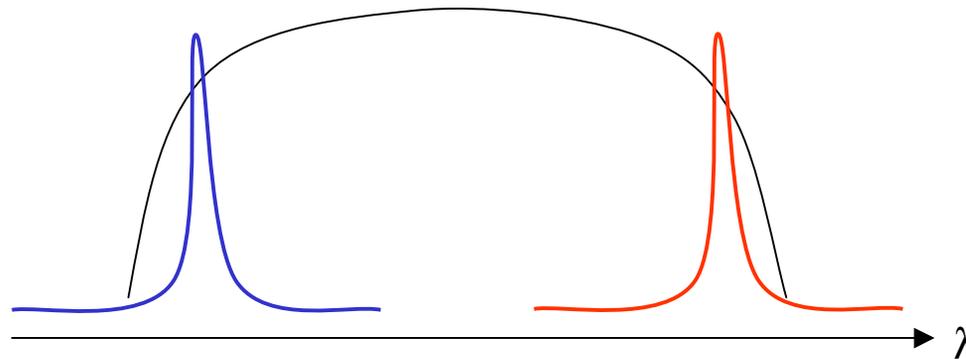
# Injection Locking Range in DBR



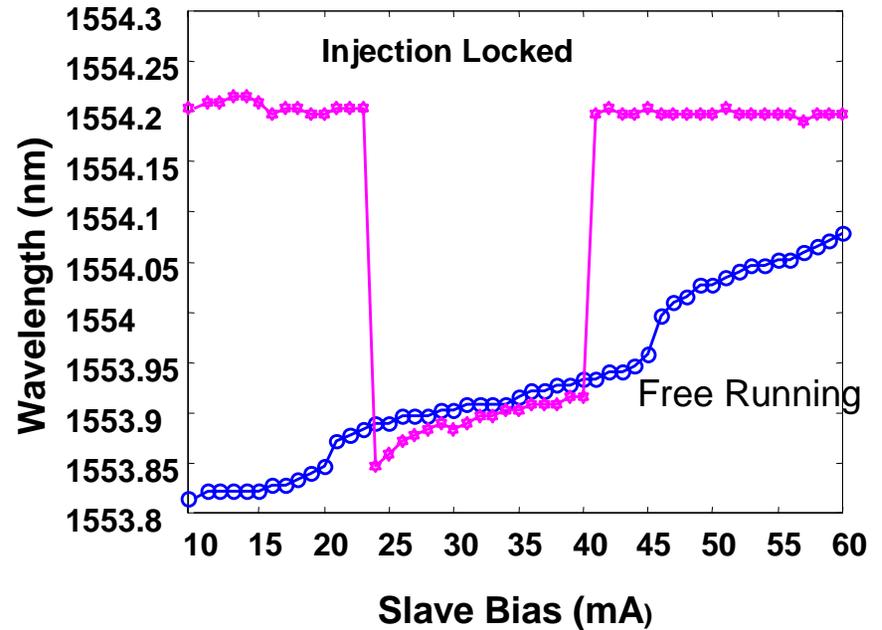
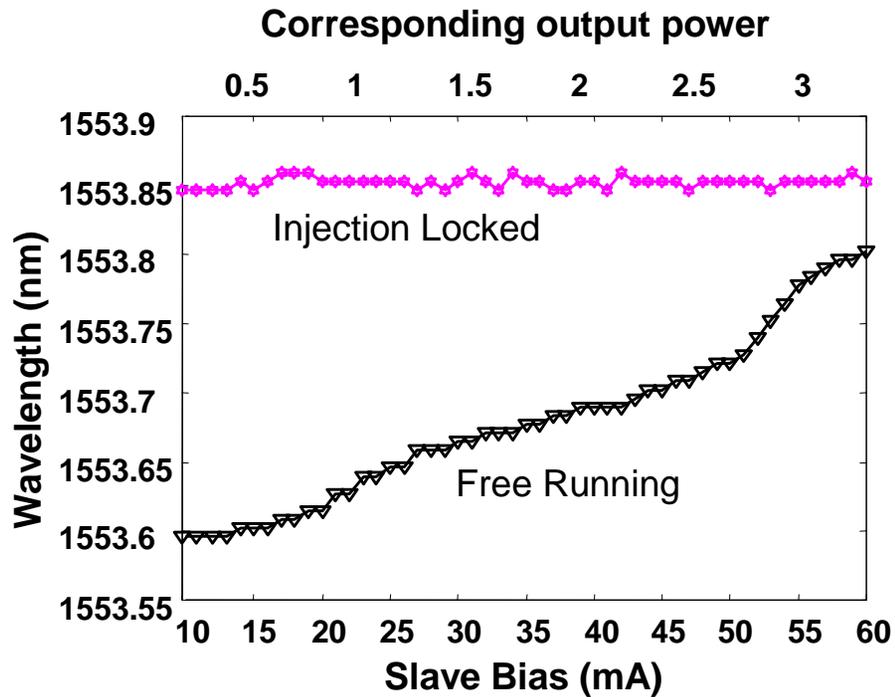
Short wavelength side



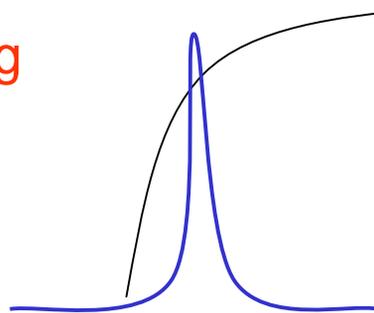
Long wavelength side



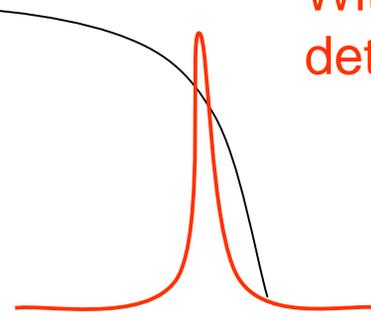
# Adiabatic Chirp Reduction



With optimal  
detuned loading



Without optimal  
detuned loading



# Summary: Bipolar Cascade

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- **Tunnel junction**
  - Developed model of tunneling current
  - Confirmed predictions with measurements in GaAs
  - Theory transportable to InP
- **Fiber coupling**
  - Evaluated alternate designs
  - Selected ARROW
  - Model predicts over 60% fiber coupling from 3 junction cascade (  $\Rightarrow$   $\sim$  150% fiber coupled quantum efficiency)
- **Material growth and characterization**
  - Achieved high doping for tunnel junctions in InP/InGaAsP by low-temperature Be doping in MBE
  - Completed InP/InGaAsP process development and active region characterization

# Summary: Resonant Modulation

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- **Modeling**
  - **Developed model for detuned loading and injection locking**
    - **Predicted results match well with experimental data**
  - **Model for resonant modulation still incomplete**
    - **For example model does not predict wide locking range on “right” side of DBR**
- **Experimental**
  - **Demonstrated injection locking over wide bias range (0.1 – 3 mW)**
  - **Enhanced modulation bandwidth by 75% (28 GHz) and reduced dynamic chirp**
  - **Eliminated adiabatic chirp**



# Outline



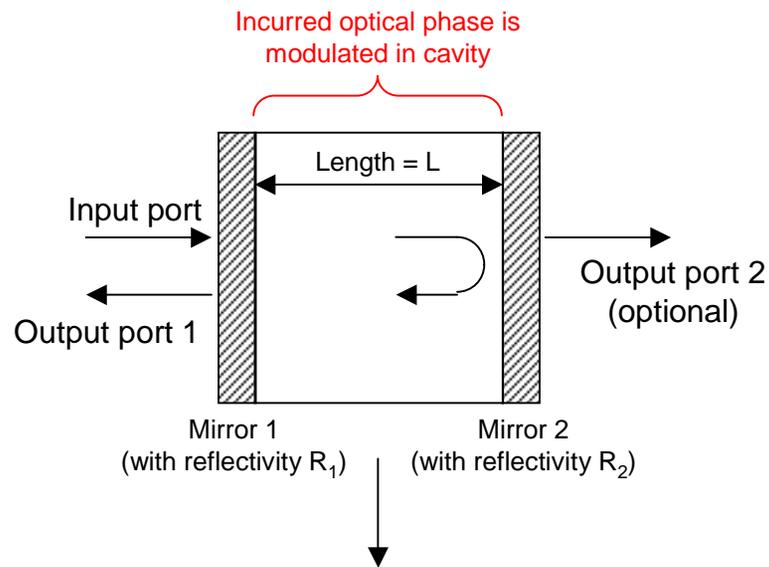
- Background
- Cascade Laser Development
- ➔ • Resonant Modulator Performance Tradeoffs
  - Modeled performance of simple resonant interferometric modulator
  - Cascaded resonant interferometric modulator (Sarnoff idea)
  - Modeled performance of modulators with combined interferometric and guide/antiguide effects
- Noise/Intermodulation Test Rack
- Summary



# Performance of Resonant Modulators

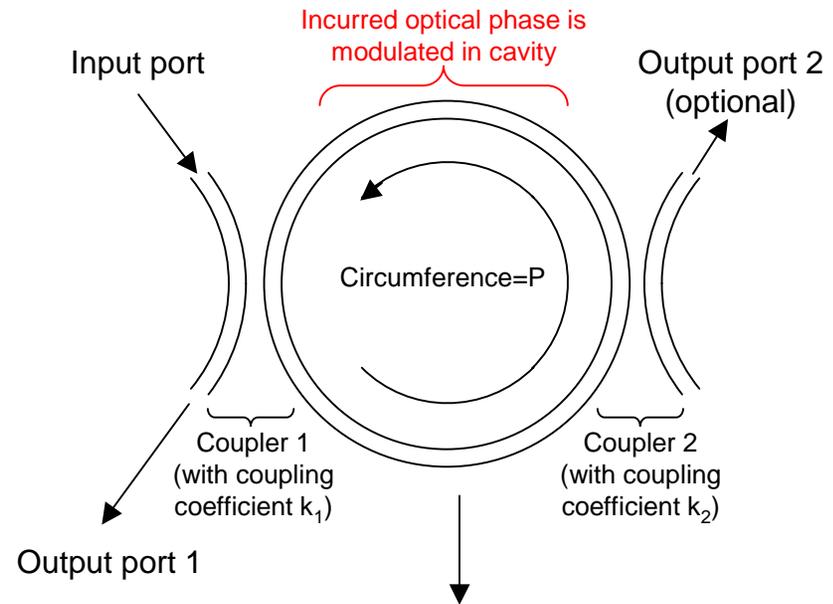


## Fabry-Perot



$R_1$ ,  $R_2$ , and  $L$  determine modulator performance

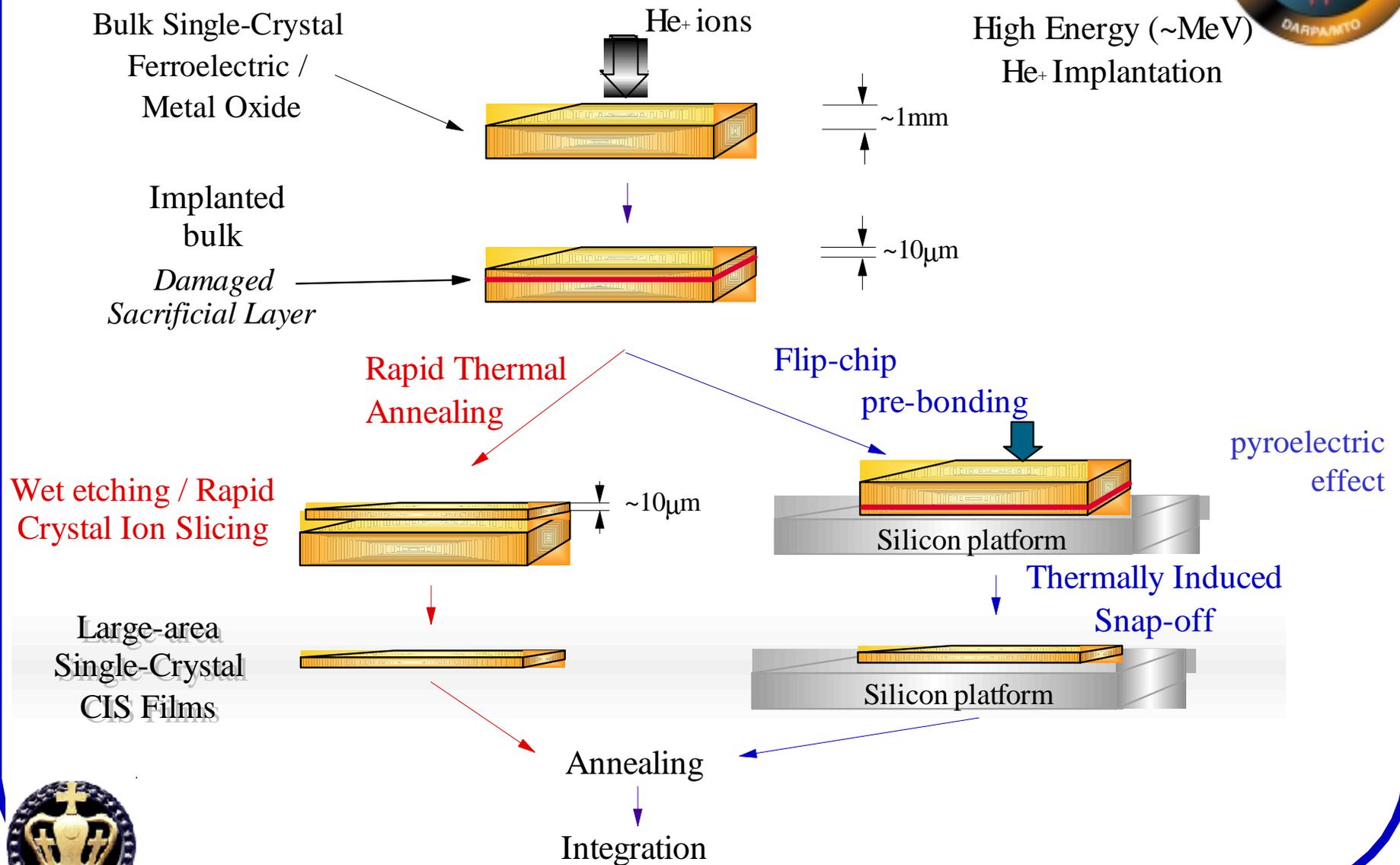
## Coupled Micro-ring Resonator



$k_1$ ,  $k_2$ , and  $P$  determine modulator performance

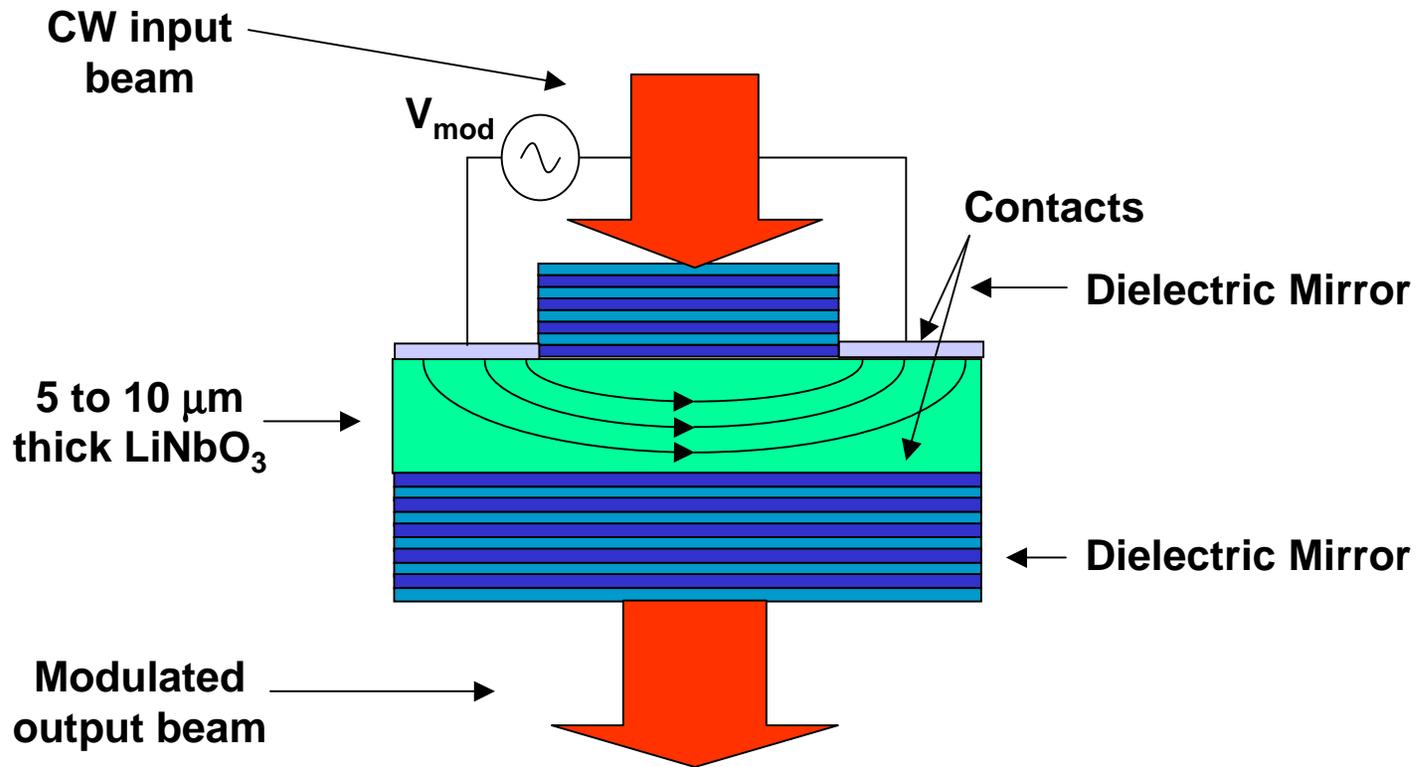


# Crystal Ion Slicing (CIS)





# Vertical Fabry-Perot Modulator in x-cut Crystal-Ion-Sliced Lithium Niobate



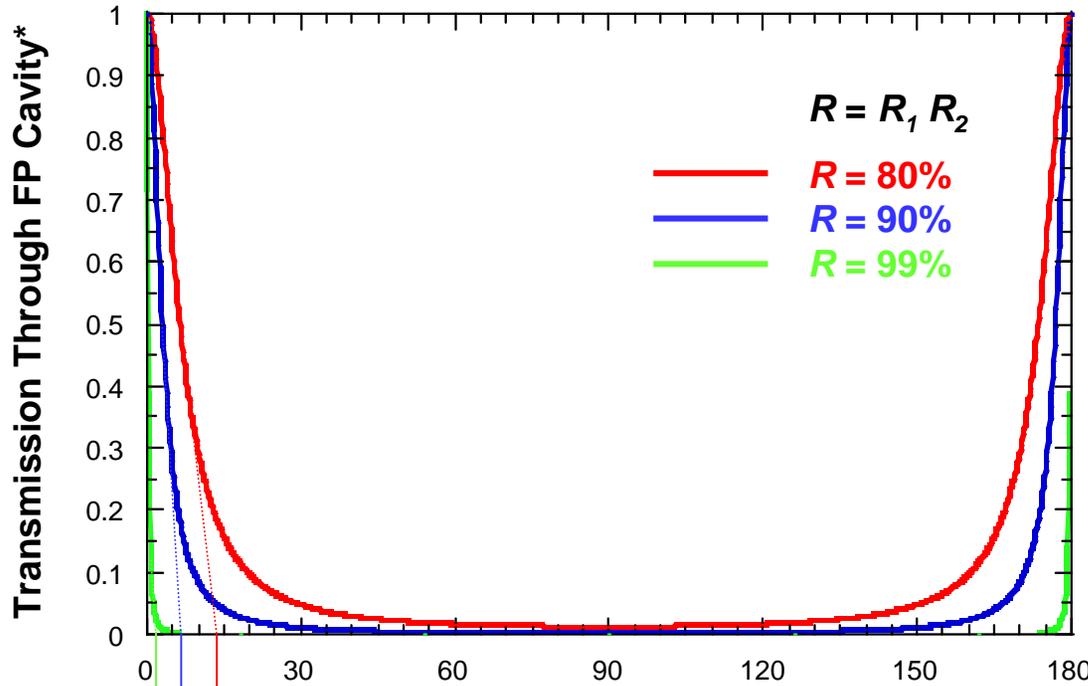
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# Fabry-Perot Modulator Performance



$V_{\pi,eq}$  Decreases with Increasing Mirror Reflectivities



$$*T(\phi) \equiv \frac{P_{out}}{P_{in}} = \frac{(1-R)^2}{(1-R)^2 + 4R \sin^2(\phi)}$$

$V_{\pi,eq} \equiv V_{\pi}$  that a MZ must exhibit to have same slope efficiency

$$= \pi \left. \frac{\partial P_{out}}{\partial v_m} \right|_{P_{out}=0.5 P_{in}, v_m=0} = \pi V_{mod}$$

$\phi$  = Optical Phase Shift Incurred in One Pass Through FP Cavity (°)



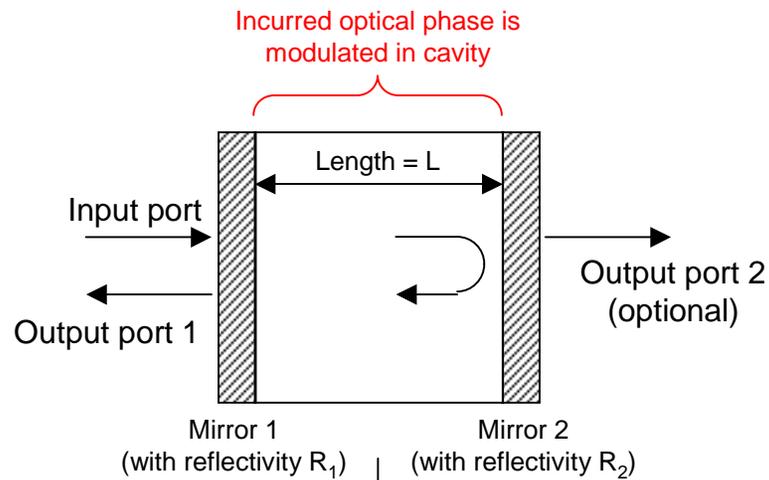
Photonic Systems, Inc.



# Performance of Resonant Modulators

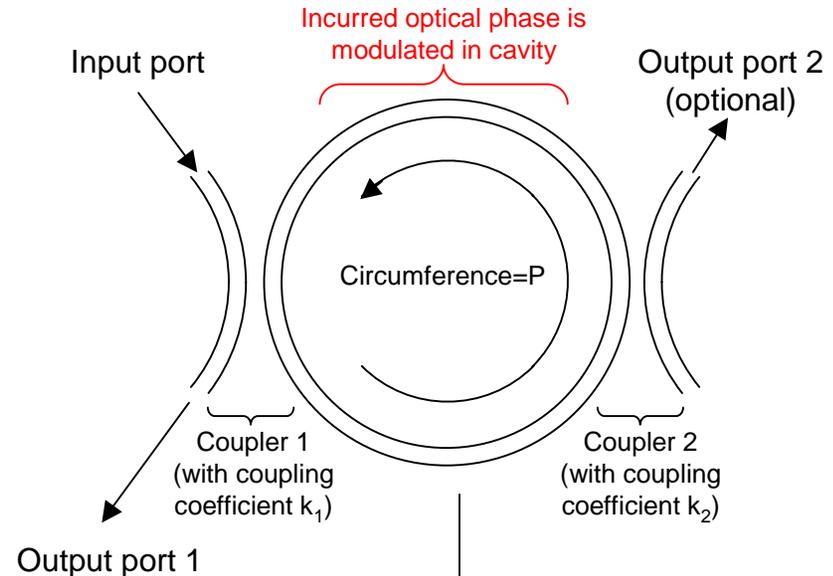


## Fabry-Perot



$$\tau \approx \frac{2 n L}{c (1 - \sqrt{R_1 R_2})}$$

## Coupled Micro-ring Resonator



$$\tau \approx \frac{n P}{c |k_1 k_2|}$$

Photon lifetime  $\tau$  determines modulator performance

For either resonant interferometer,

$$V_{\pi,eq} \propto \frac{1}{\tau}$$

$$f_{3dB} \propto \frac{1}{\tau}$$

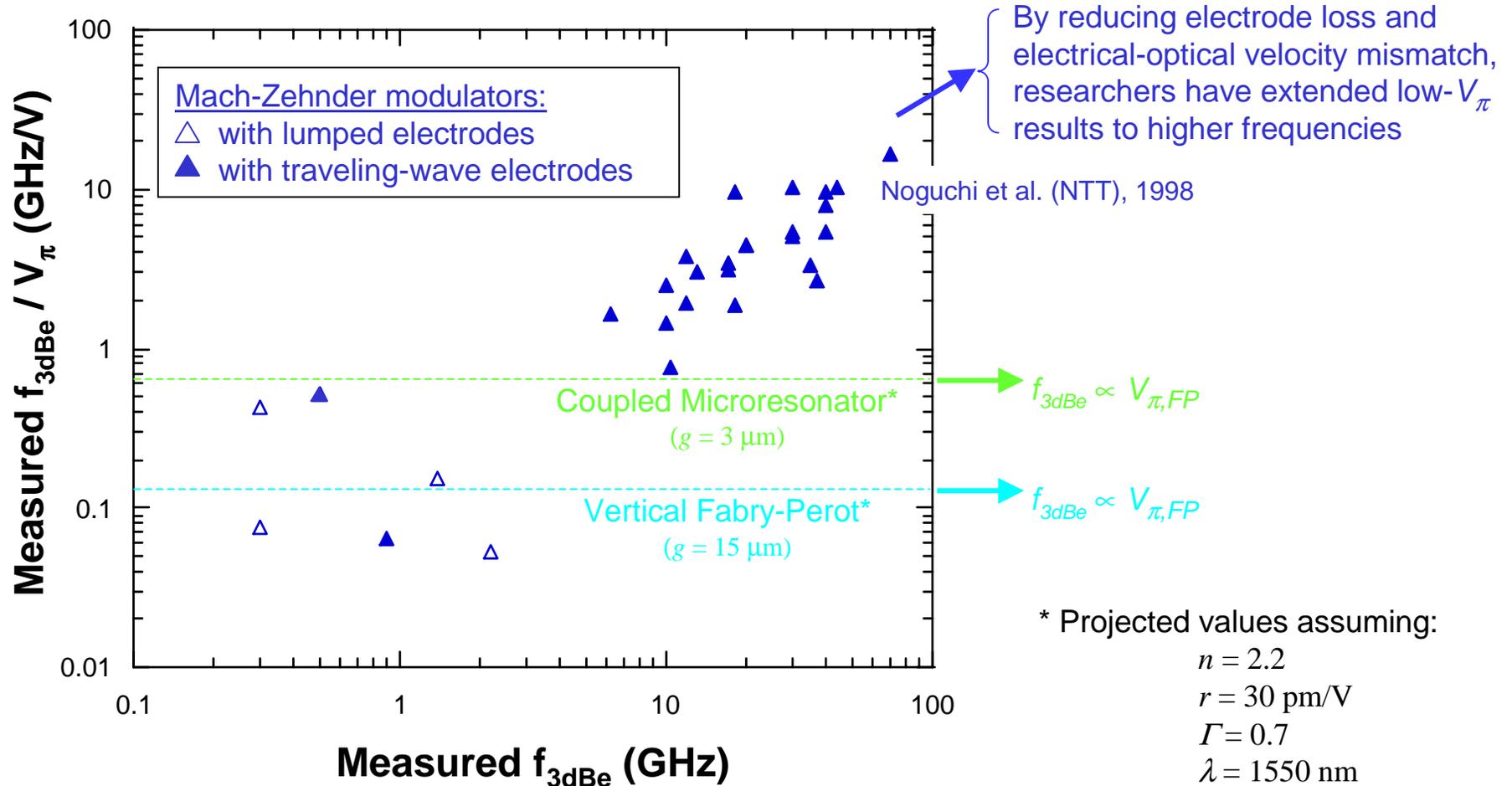
$$\frac{f_{3dB}}{V_{\pi,eq}} \approx \frac{\sqrt{\sqrt{2}-1} n^2 r \Gamma c}{2\pi \lambda g}$$

Independent of  $R$  and  $L$ , or  $k$  and  $P$

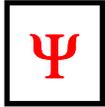
**Photonic Systems, Inc.**



# Projected Resonant Interferometric LiNbO<sub>3</sub> Modulator Results vs. MZ



Photonic Systems, Inc.



# Outline

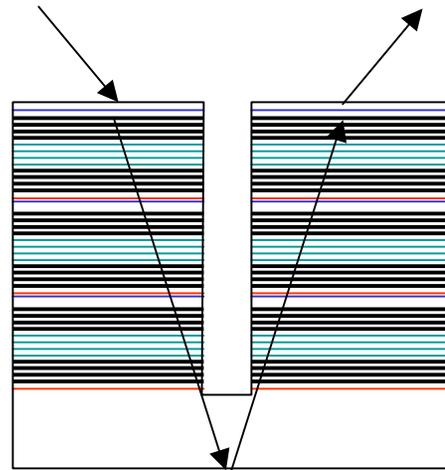


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- **Resonant Modulator Performance Tradeoffs**
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  - Modeled performance of modulators with combined interferometric and guide/antiguide effects
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# 6x better multi-vertical Cavity Modulator



- Each stage equivalent to a 12  $\mu\text{m}$  diameter ring resonator in photon lifetime
- For capacitance equivalent to a 1  $\mu\text{m}$  wide ring resonator, need diameter of 10  $\mu\text{m}$  or less
- Must use electrorefractive configuration.
- Cannot use electroabsorption effect due to destruction of resonance



Photon lifetime of ~4 psec per stage\*

3 stages with double pass and individual electrical contact to each stage;

Must install RF delay lines between stages.

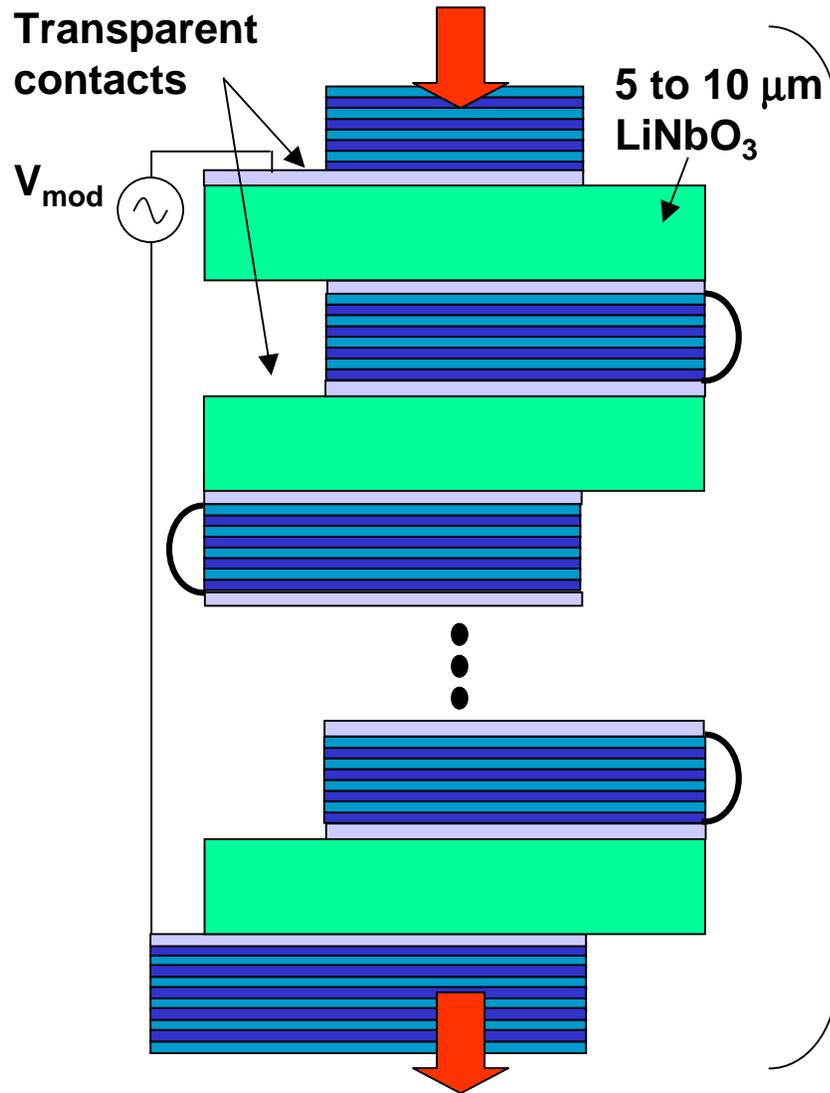
*6x lower  $V_{\pi}$  from this arrangement*

\* 2  $\mu\text{m}$  [height]  $\times$  200 [finesse]  $\times$  0.01 psec/ $\mu\text{m}$ ;  
N.B.: equivalent to a 400 mm straight modulator

$$f_{3\text{dB}} = 1/(2\pi \times 4 \text{ [psec]}) = 40 \text{ GHz}$$



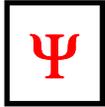
# Sarnoff Cascaded Fabry-Perot Modulator in z-cut CIS Lithium Niobate



A device conceptually equivalent to this could have up to 100 cascaded FP's in 1 cm:

$$\frac{f_{3dBc}}{V_{\pi,eq}} \approx 10 \text{ GHz/V}$$

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# Outline



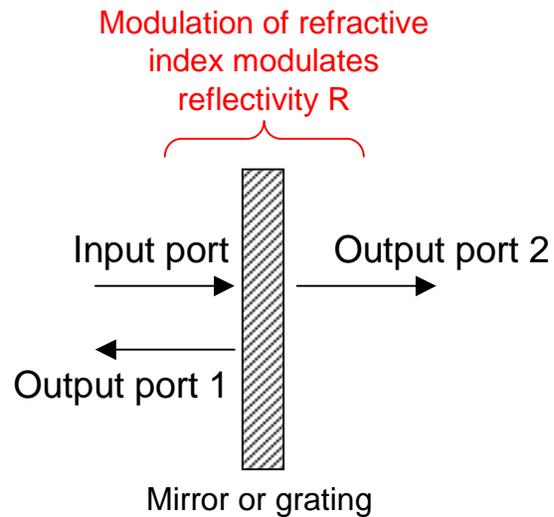
- **Background**
- **Cascade Laser Development**
- **Resonant Modulator Performance Tradeoffs**
  - Modeled performance of simple resonant interferometric modulator
  - Cascaded resonant interferometric modulator (Sarnoff idea)
  - ➔ – Modeled performance of modulators with combined interferometric and guide/antiguide effects
- **Noise/Intermodulation Test Rack**
- **Summary**



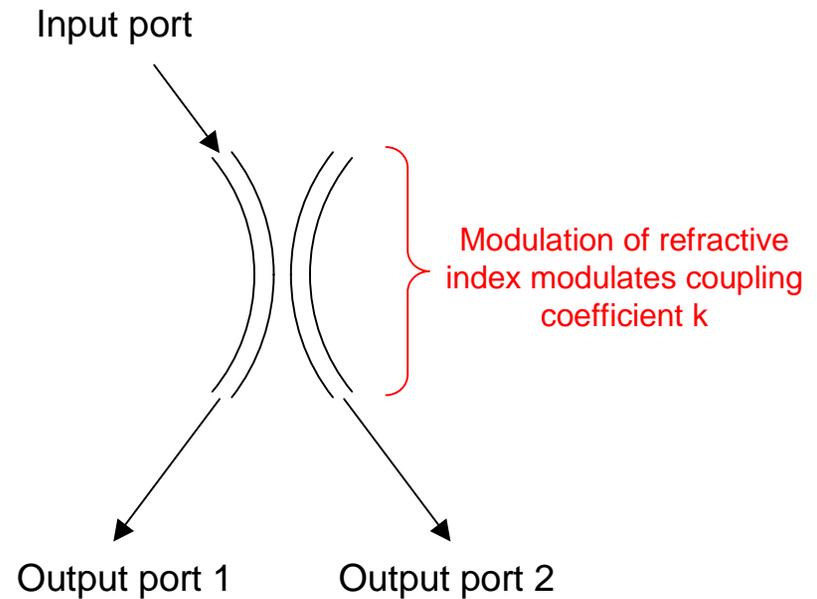
# Guide/Antiguide Modulators



## Mirror type



## Coupler type

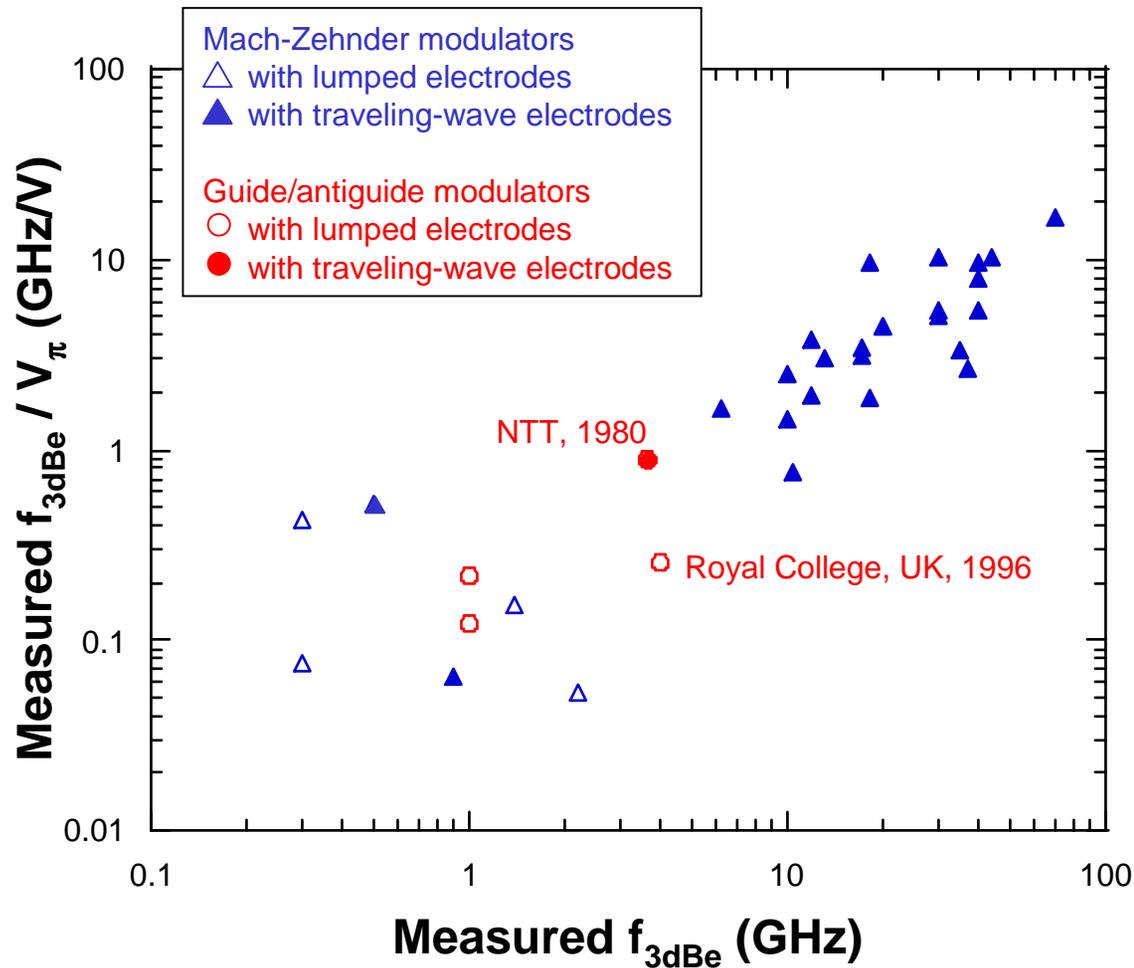


$$R \Leftrightarrow 1 - |k|^2$$



# LiNbO<sub>3</sub> Guide/Antiguide Modulators

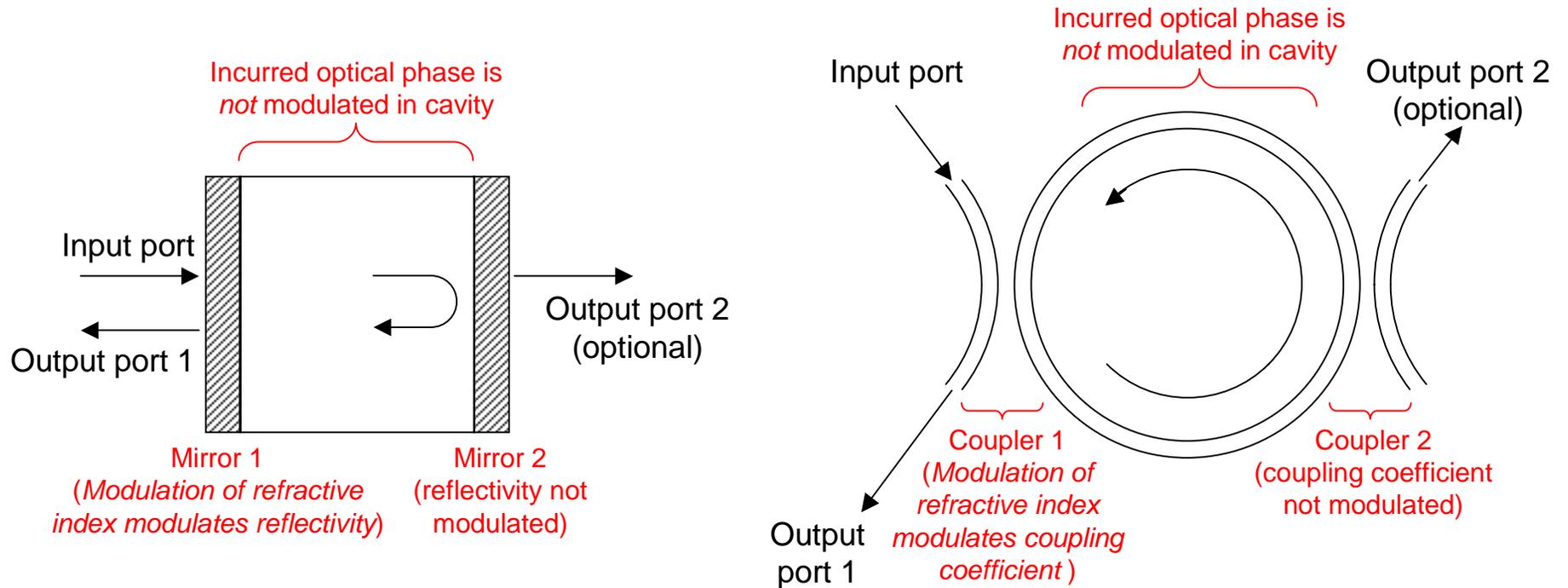
## How They Have Stacked Up Against LiNbO<sub>3</sub> MZ's



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# Modulators with Combined Interferometric and Guide/Antiguide Effects

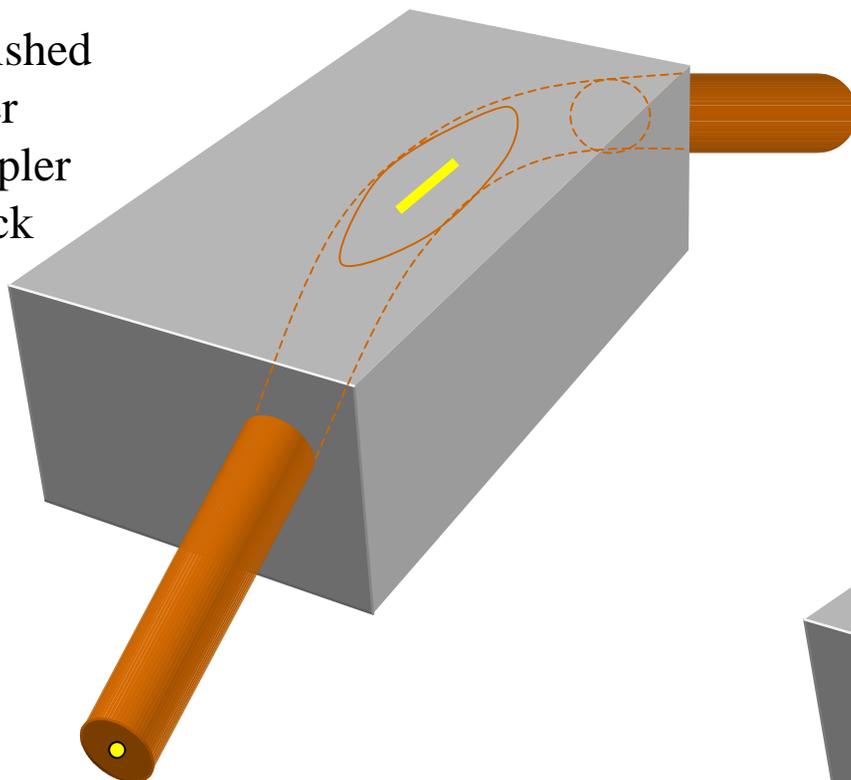


**We are investigating the efficiency-bandwidth tradeoffs of these designs.**

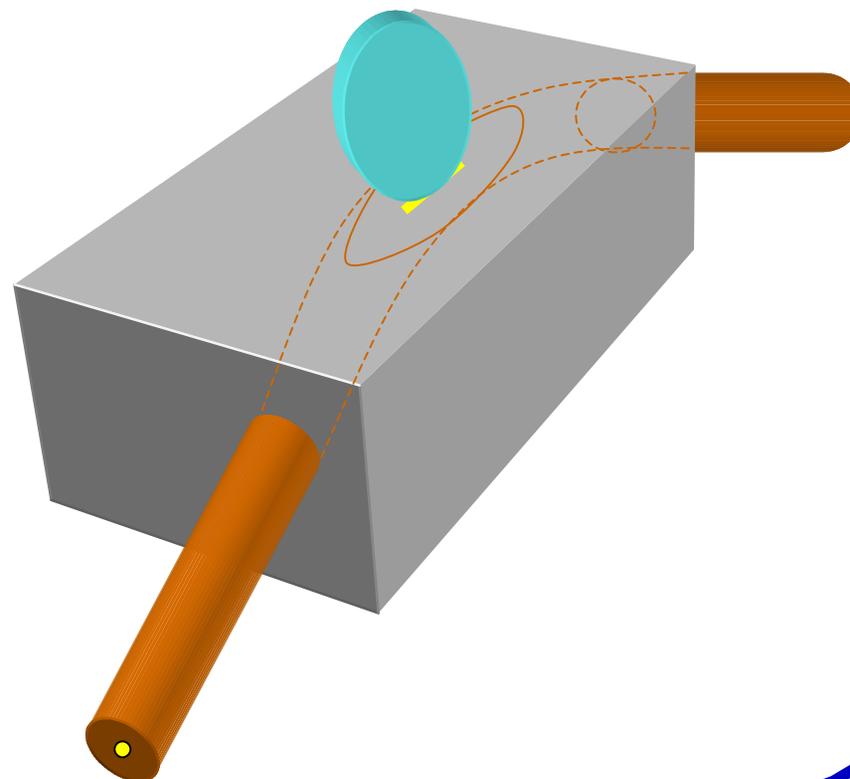
# Implementation of Disk Resonator Device



Polished  
fiber  
coupler  
block

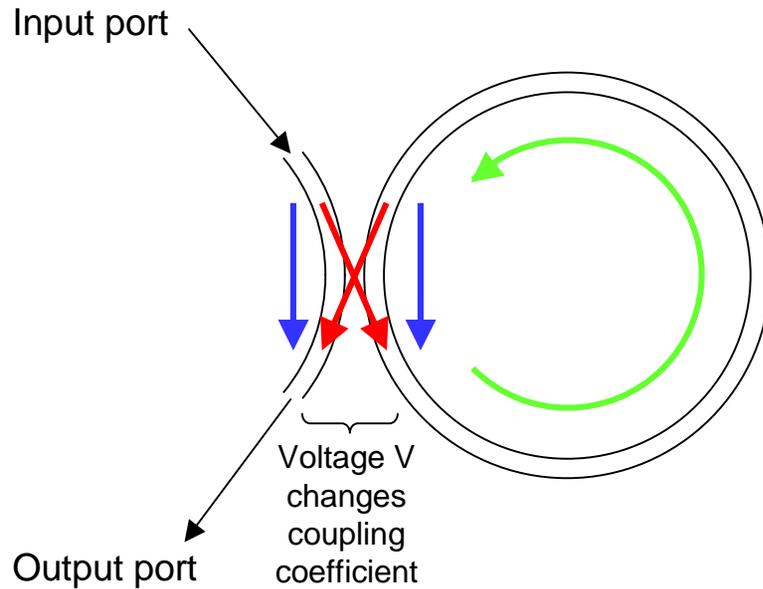


Evanescent  
coupling to  
vertical disk





# Analysis of Disk Resonator Modulator



*Cross state:*  $C(V) = \frac{\sin^2 \left( \frac{\pi}{2} \sqrt{1 + 3 \left( \frac{V}{V_s} \right)^2} \right)}{1 + 3 \left( \frac{V}{V_s} \right)^2}$

*Bar state:*  $B(V) = 1 - C(V)$

*Delay:*  $D = e^{j2\pi \frac{P}{\lambda}}$

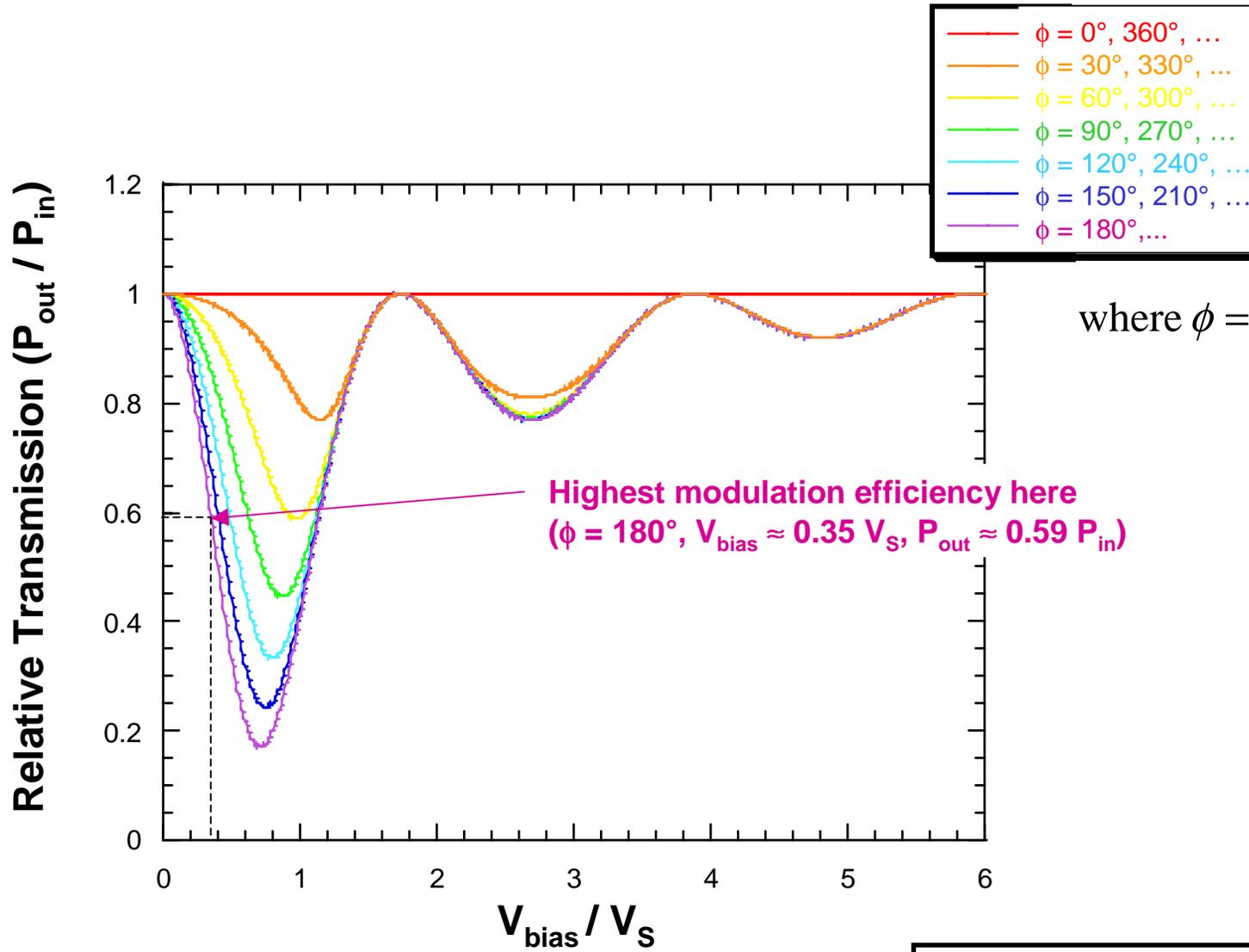
$$V_s = \frac{2\sqrt{3} g \lambda}{n^3 r L}$$

*Transmission Characteristic:*  $T(V) = [B(V)] + [C(V) \cdot \overset{\downarrow}{D} \cdot C(V)] + [C(V) \cdot \overset{\downarrow}{D} \cdot B(V) \cdot \overset{\downarrow}{D} \cdot C(V)] + [C(V) \cdot \overset{\uparrow}{D} \cdot B(V) \cdot \overset{\uparrow}{D} \cdot B(V) \cdot \overset{\uparrow}{D} \cdot C(V)] + K$

$$= B(V) + \frac{[C(V)]^2 D}{1 - B(V) \cdot D}$$



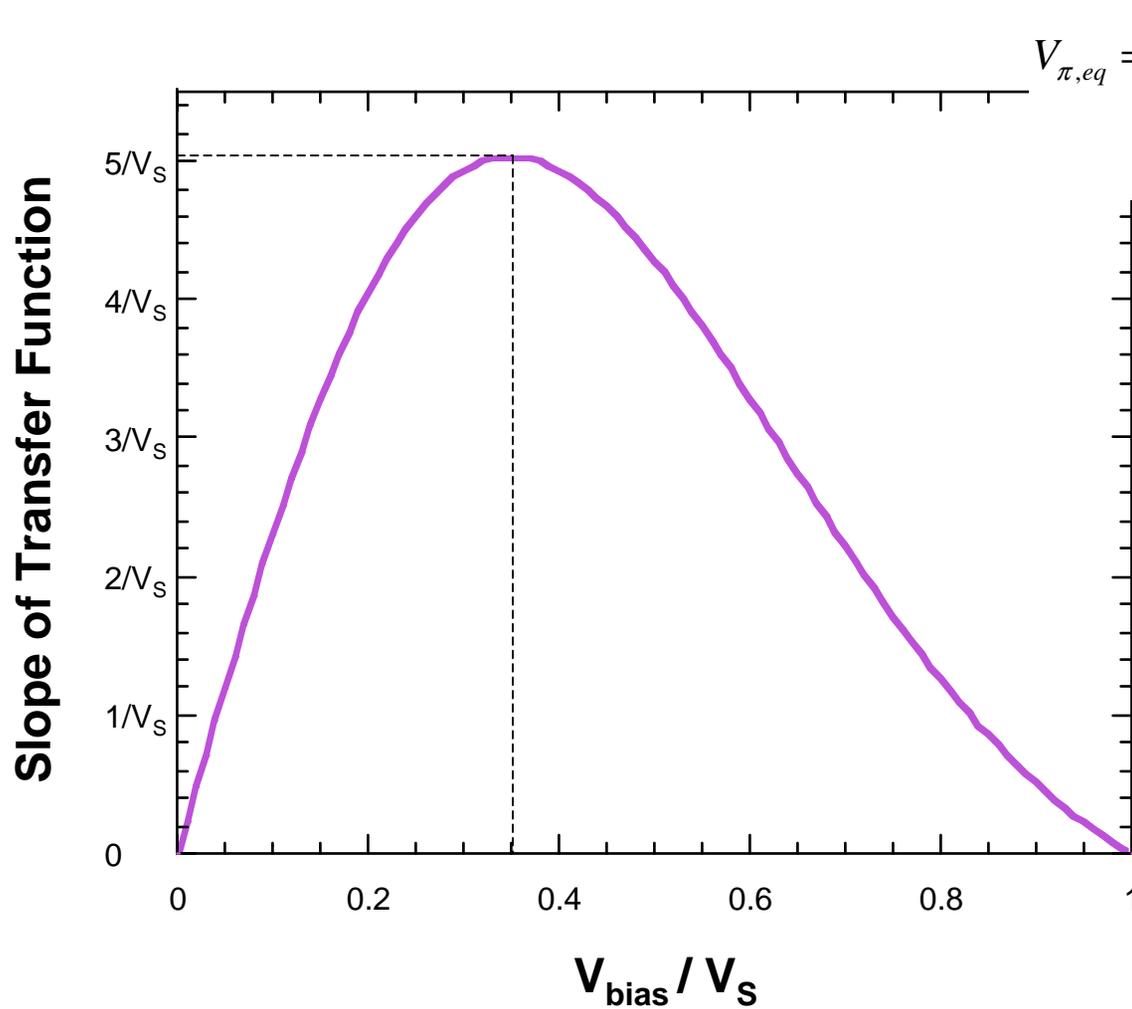
# Analysis of Disk Resonator Modulator



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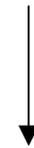
# Analysis of Disk Resonator Modulator



$$V_{\pi,eq} = \pi \frac{P_{out}}{\left. \frac{\partial P_{out}}{\partial v_m} \right|_{P_{out} \approx 0.59 P_{in}, v_m=0}} \approx \pi \frac{0.59}{5/V_S},$$

where  $V_S = \frac{2\sqrt{3} g \lambda}{n^3 r \Gamma L}$

and  $f_{3\text{dBe}} \approx \frac{\sqrt{\sqrt{2}-1}}{2\pi} \frac{c}{nP} B(V)$

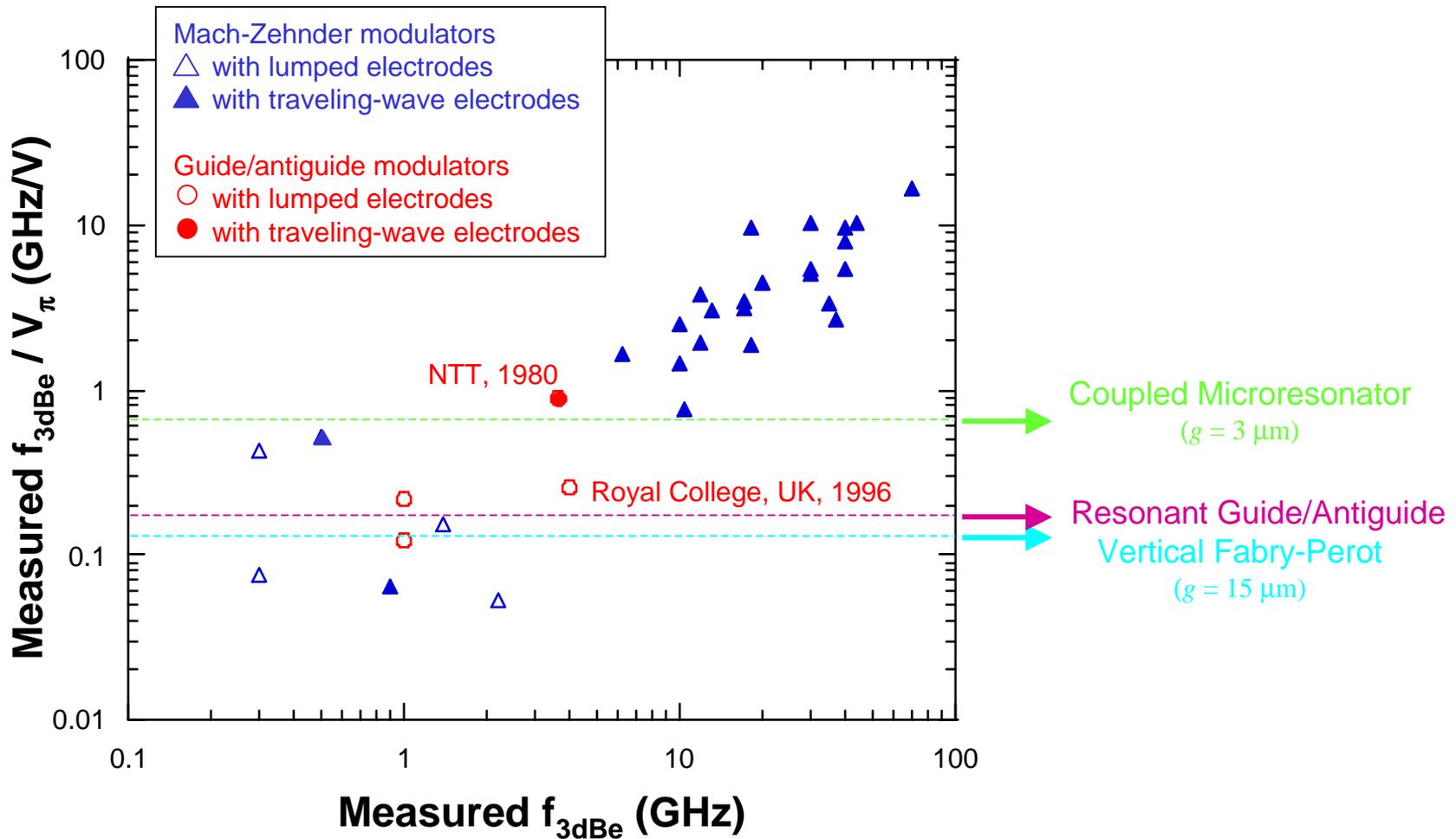


SO  $\frac{f_{3\text{dBe}}}{V_{\pi,eq}} \approx \frac{n^2 r \Gamma c L}{4\pi \lambda g P} B(V)$

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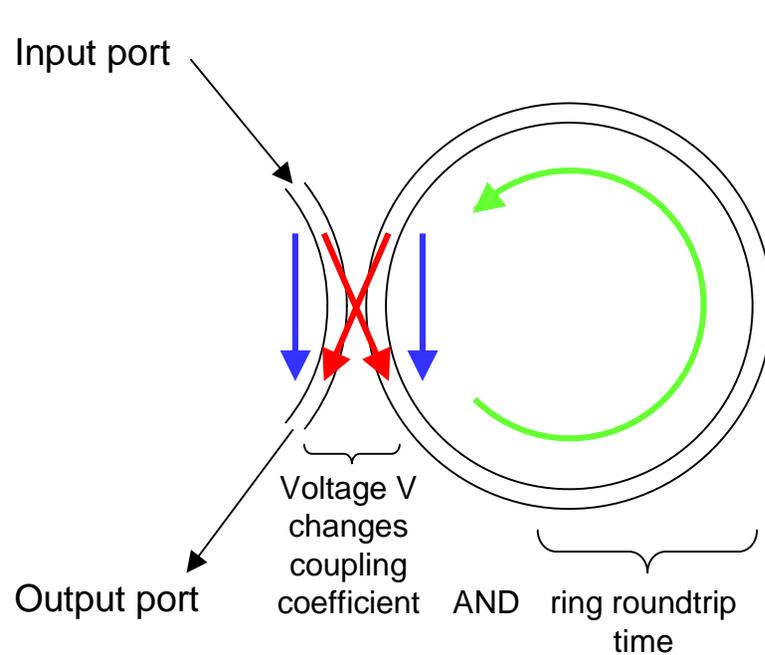
# Projected Resonant Guide/Antiguide LiNbO<sub>3</sub> Modulator Result vs. MZ



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# Analysis of Disk Resonator Modulator with Cascaded Modulation Effects



*Cross state:*  $C(V) = \frac{\sin^2 \left( \frac{\pi}{2} \sqrt{1 + 3 \left( \frac{V}{V_s} \right)^2} \right)}{1 + 3 \left( \frac{V}{V_s} \right)^2}$

*Bar state:*  $B(V) = 1 - C(V)$

*Delay:*  $D(V) = e^{j2\pi m(V) \frac{P}{\lambda}}$

$$V_s = \frac{2\sqrt{3} g \lambda}{n^3 r L}$$

*Transmission Characteristic:*  $T(V) = B(V) + \frac{[C(V)]^2 D(V)}{1 - B(V) \cdot D(V)}$



# Analysis of Disk Resonator Modulator with Cascaded Modulation Effects



$$\text{Slope of transfer function} = 2 \frac{C^3(C-1) \frac{\pi}{V_\pi} \sin \phi + (3C^2 - 8C + 4) \frac{\partial C}{\partial v} \cos \phi - (C^2 - 4C + 2) \frac{\partial C}{\partial v} - 2(C-1)^2 \frac{\partial C}{\partial v} \cos^2 \phi}{\sqrt{[(C^2 - 2C + 2) + 2(C-1)\cos \phi]^3 [(5C^2 - 6C + 2) - (4C^2 - 6C + 2)\cos \phi]}}$$

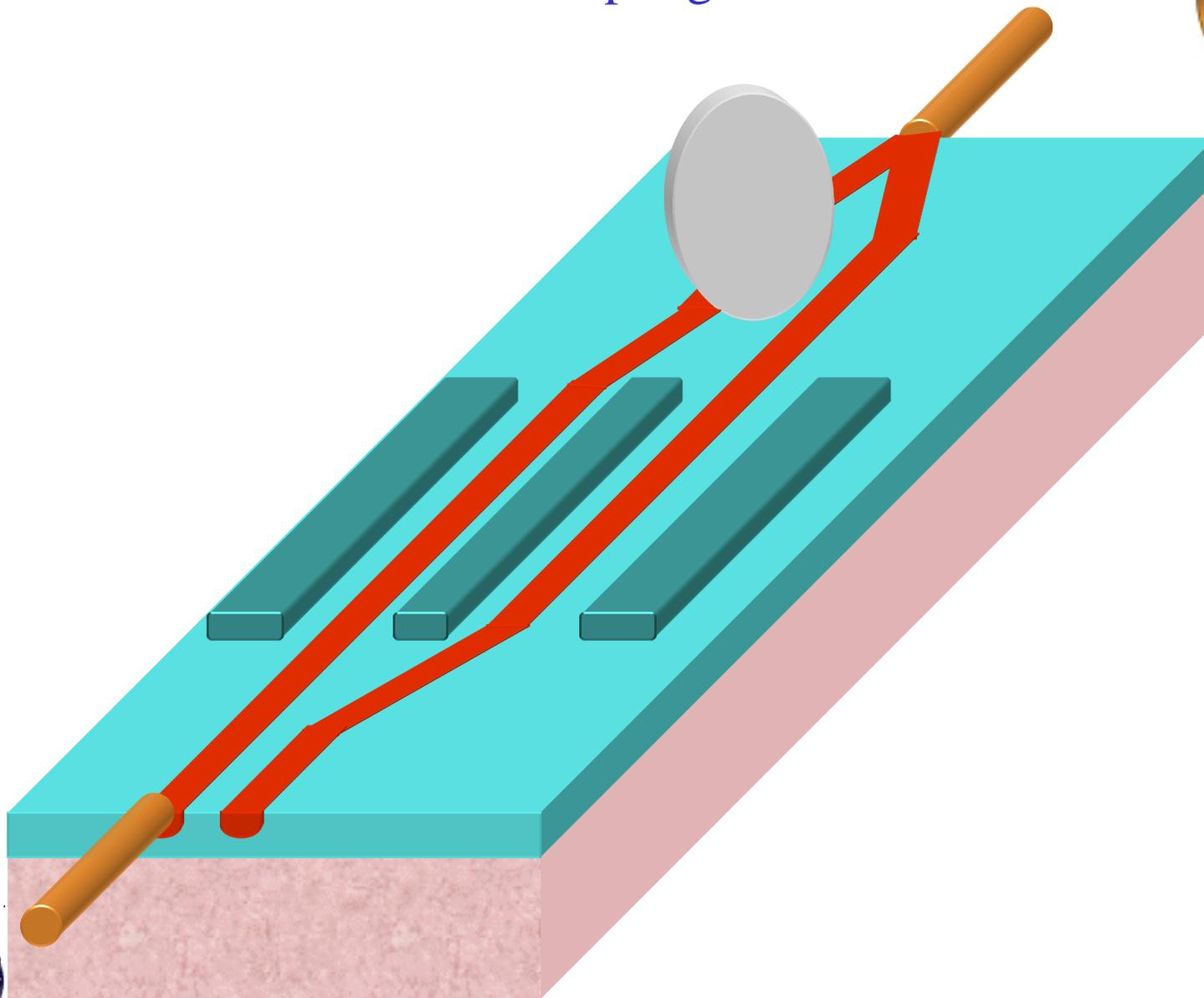
where  $\phi = 2\pi n \frac{P}{\lambda}$

$$C = \frac{\sin^2 \left( \frac{\pi}{2} \sqrt{1 + 3 \left( \frac{V}{V_s} \right)^2} \right)}{1 + 3 \left( \frac{V}{V_s} \right)^2}$$

- Three degrees of freedom:
1. Resonator roundtrip bias  $\phi$
  2. Directional coupler bias  $V$
  3. Ratio of  $V_s$  to  $V_\pi$

$$\text{and } \frac{\partial C}{\partial v} = \frac{3V}{V_s^2} \frac{1}{1 + 3 \left( \frac{V}{V_s} \right)^2} \left[ \frac{\pi}{2} \sqrt{1 + 3 \left( \frac{V}{V_s} \right)^2} \sin \left( \pi \sqrt{1 + 3 \left( \frac{V}{V_s} \right)^2} \right) - 2 \sin^2 \left( \frac{\pi}{2} \sqrt{1 + 3 \left( \frac{V}{V_s} \right)^2} \right) \right]$$

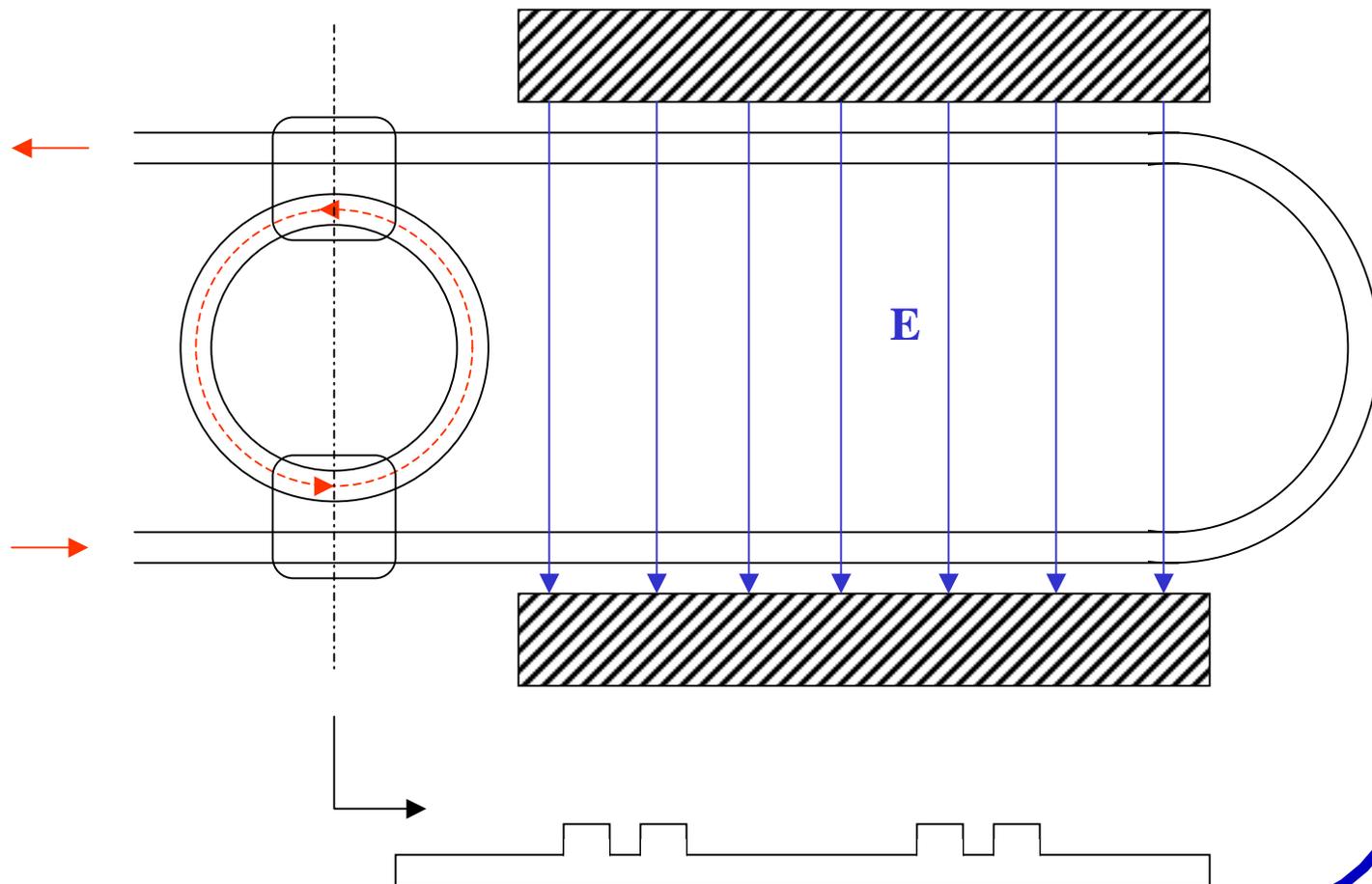
# Mach-Zehnder based coupling variation





# Interferometric Coupling Modulation

Practical implementation:



~ also version with TW electrodes ~





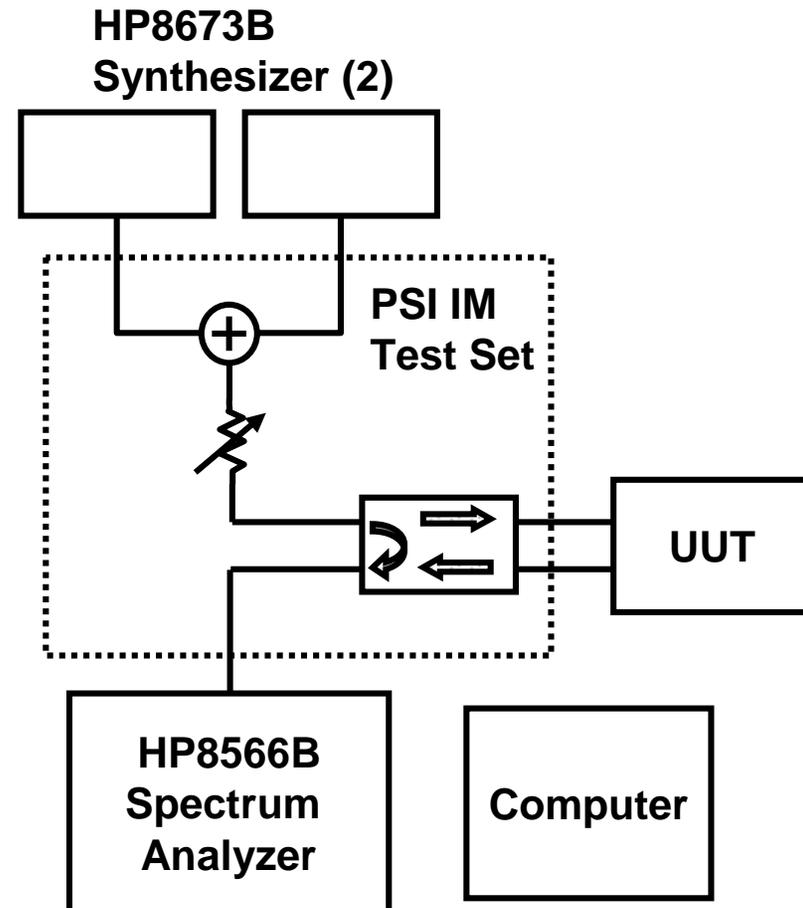
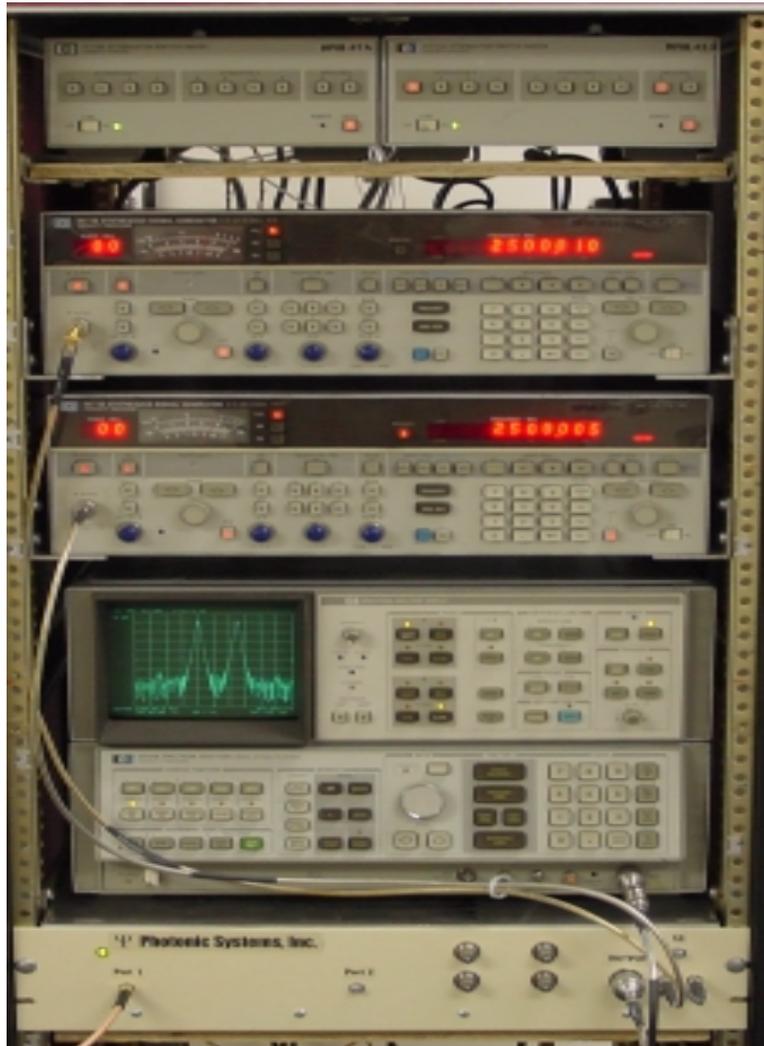
# Outline



- 
- Background
  - Cascade Laser Development
  - Resonant Modulator Performance Tradeoffs
  - ➔ • Noise/Intermodulation Test Rack
  - Summary



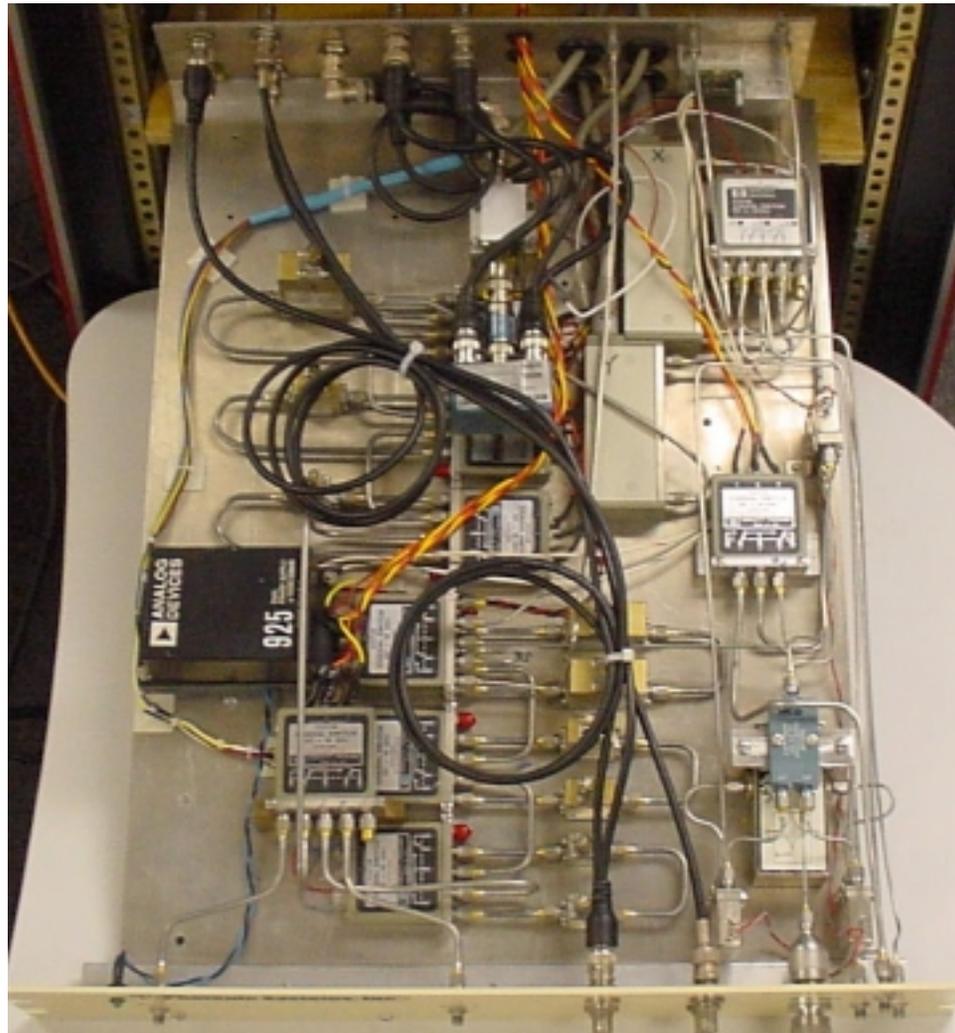
# PSI Noise and Distortion Measurement System



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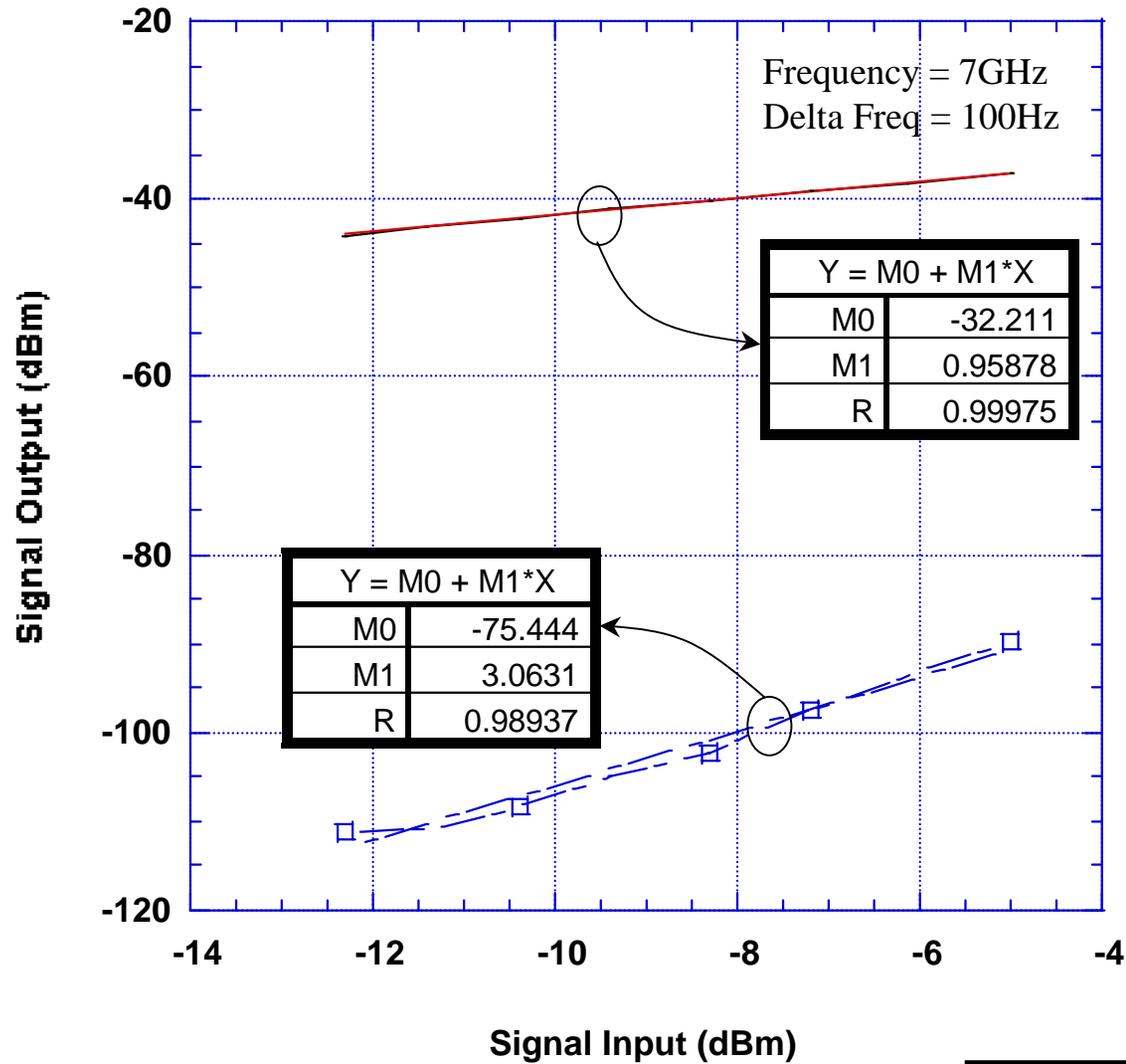
# PSI Noise/IM Test Set



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# 3<sup>rd</sup> Order IM Measurements External Modulation Link



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# Outline



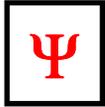
- **Background**
- **Cascade Laser Development**
- **Resonant Modulator Performance Tradeoffs**
- **Noise/Intermodulation Test Rack**
- • **Summary**



# Summary



- **Cascade Laser for Direct Modulation Links**
  - Validated model of low-wavelength tunnel junction measurements in GaAs is being used to design 1.55  $\mu\text{m}$  devices in InP
  - ARROW waveguide design is being applied to solve fiber coupling issue
  - Fiber-coupled effective quantum efficiency of 150% predicted for 3-laser cascade
  - Detuned loading and injection locking yield very high bandwidth (demonstrated 28 GHz) and low chirp
- **Resonant Modulators for External Modulation Links**
  - Investigating several designs to exploit Columbia crystal ion slicing technique
  - So far, all resonant structures have yielded efficiency-bandwidth tradeoffs inferior to traveling-wave MZs
  - Sarnoff cascaded traveling-wave FP concept is being investigated as a solution (however implementation is challenging)
  - Structures that combine resonance with guide/antiguide effects may yield alternative solutions



# Most Significant Accomplishment

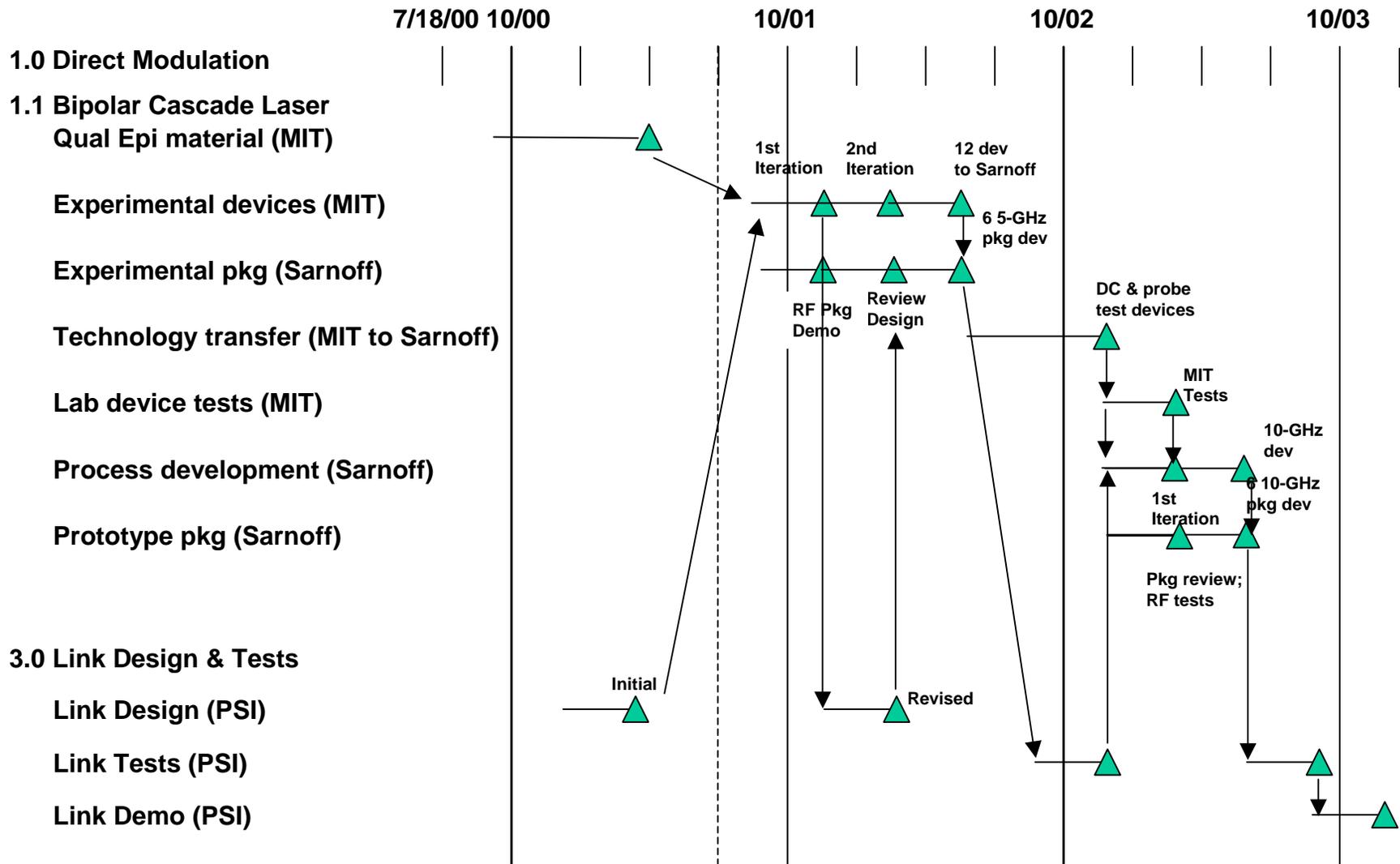
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- **Demonstration:**
  - **28 GHz direct modulation of resonant-modulation laser with zero adiabatic chirp and very low dynamic chirp**



# Program Roadmap Cascade Laser

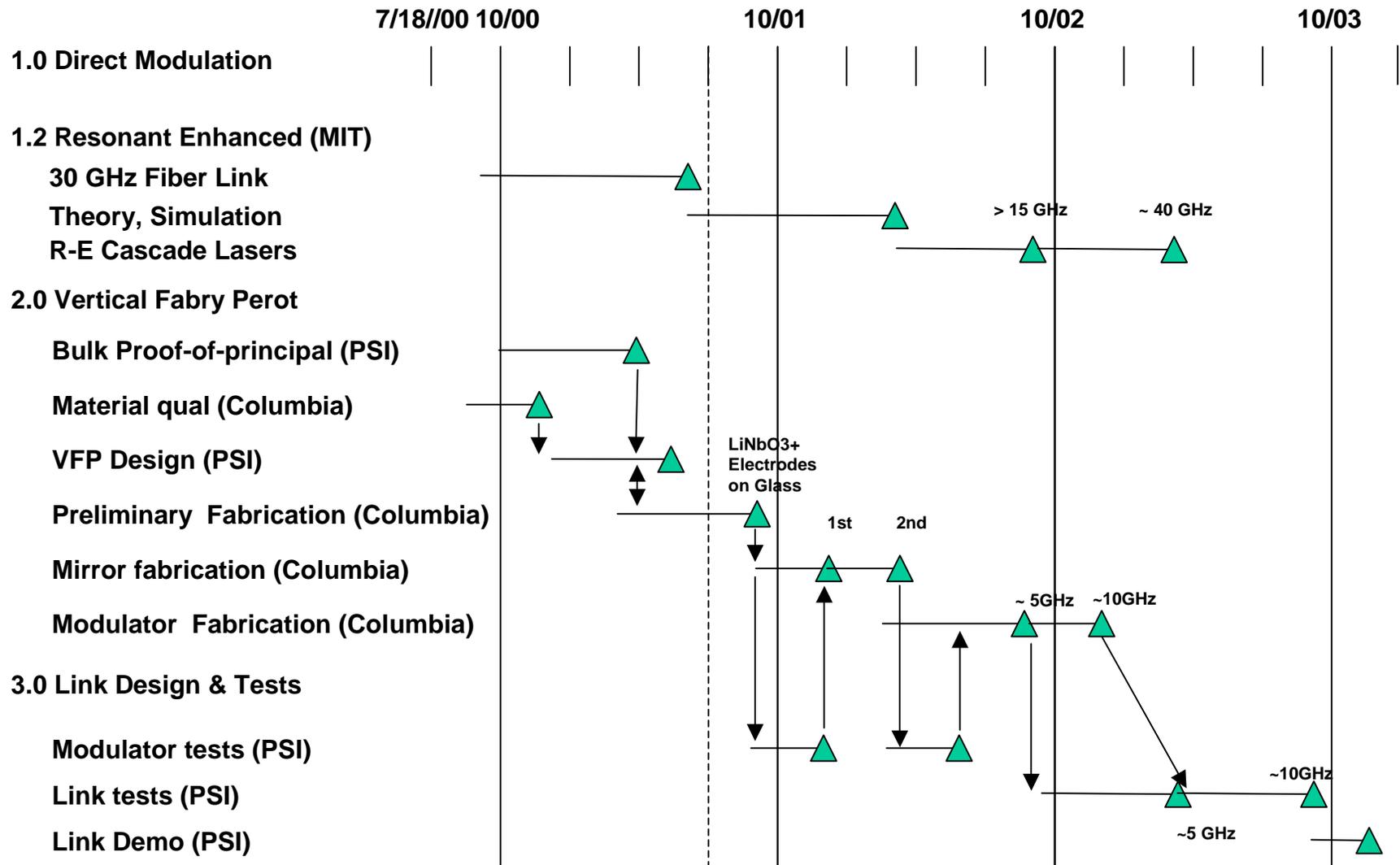


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# Program Roadmap

## Resonantly Enhanced & External Modulation



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